## Campsie Stage 2 Traffic Analysis

Mesoscopic Transport Modelling Report


Prepared by: Stantec Australia Pty Ltd Pty Ltd for Canterbury-Bankstown City Council on 14/02/2022
Reference: N205150
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# Campsie Stage 2 Traffic Analysis 

Mesoscopic Transport Modelling Report Draft Final Report

Client: Canterbury-Bankstown City Council
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## 1. INTRODUCTION



### 1.1. Background

Canterbury-Bankstown City Council (Council) has developed a Local Strategic Planning Statement, Connective City 2036, that recognises Campsie as a Strategic Centre, evolving into an important health and lifestyle precinct for the city. The delivery of Sydney Metro South-West Services, investment in a new cultural and civic hub and renewal in the centre will provide a catalyst for the realisation of the vision for Campsie. Campsie's connectivity will change with the opening of Sydney South West Metro services, connecting it to the City within 20 minutes, and to new centres it has not been connected to directly in the past, such as North Sydney, Chatswood, Macquarie Park and North-West Sydney. Campsie is located on the banks of the Cooks River and is located approximately 12 kilometres south-west of Sydney.

Beamish Street functions as a spine road that runs north-south through the Campsie Town Centre providing a key connection between the town centre, Campsie train station and key arterial roads such as Georges River Road in the north and Canterbury Road in the south. The majority of the commercial development such as small retailers, food outlets and other various small businesses are concentrated on either side of Beamish Street.

Council has developed a draft masterplan that focuses on capitalising this opportunity and recognises the presence of the hospital and embrace its unique position next to the river to create a health and lifestyle hub. This masterplan needs to be supported by strong evidence through transport modelling to achieve a more consistent basis for impact assessment and identification of infrastructure and service improvements required. This modelling and the draft Master Plan will inform transport and traffic network changes to be developed in the coming 10-20 years.

A robust traffic model provides the opportunity to assess the collective impacts of such infrastructure upgrades, highlight future problems, and identify mitigations which align with the aspirations of Council. Therefore, a mesoscopic (meso) model has been developed as a robust capacity forecasting tool that can provide visual and performance outputs to show the contributing factors driving infrastructure needs for planners and policy makers to modify planning scenarios.

### 1.2. Project Objective

The objective of this study is to develop a traffic model for Campsie that will provide direction for the Campsie Complete Streets Integrated Transport and Place Plan, which will result in a series of recommendations for transport, road, and public domain infrastructure to support the planned growth of the centre. Ultimately, this work will:

- assess the ability of the local transport network to accommodate the planned growth under the draft Campsie Town Centre Master Plan
- enable rapid assessment and accelerated delivery of infrastructure and land development
- provide forecasts of travel behaviour and network performance under a range of planning scenarios
- enable prioritisation of mitigation works.


### 1.3. Scope of Works

This report outlines the:

- calibration and validation process and key assumptions made to develop the existing conditions meso model
- existing conditions model results
- development of future year and options scenario meso models
- future year and options scenario model results.


### 1.4. Study Area

The proposed study area is presented in Figure 1.1 and covers the Campsie town centre. The study area extends from Canterbury Road in the south and is bounded by Cooks River in the north and east, and Burwood Road, the freight rail line and canterbury hospital in the west.

Figure 1.1: Study area extents


Base map source: Google Maps
The study area generally aligns with the study area of the Draft Campsie Master Plan with the exception of a small area south of Canterbury Road, which is shown in Figure 1.2. The Draft Master Plan shows a potential residential / commercial growth within this section and change of use from R3 to R4 zone.

Figure 1.2: Campsie Draft Master Plan study area extents


Source: Campsie Town Centre, March 2021 Master Plan, Final Draft for Exhibition.

### 1.5. Report Outline

This report sets out an overview of the meso model development process and an assessment of the existing traffic conditions. The report is divided in following sections:

- Chapter 1 Introduction
- Chapter 2 Existing Conditions
- Chapter 3 Model Assumptions
- Chapter 4 Future Year Models
- Chapter 5 Option Scenario Models
- Chapter 6 Conclusion.

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## 2. EXISTING CONDITIONS



## EXISTING CONDITIONS

### 2.1. Traffic Surveys

Comprehensive traffic data was collected to develop, calibrate, and validate the existing conditions models. A summary of the data collected is provided in Table 2.1.

Table 2.1: Traffic data summary

| Data Type | Source | Survey Dates | Survey Time |
| :--- | :--- | :--- | :--- |
| Annual Average Daily Traffic Data | Transport for NSW | 2018, 2019 | 24 hours |
| SCATS Detector Volume Data | Transport for NSW | Thursday 21/02/2019 | 24 hours |
| SCATS Signal Data | Transport for NSW | Thursday 21/02/2019 <br> Thursday 25/03/2021 | 24 hours |
| Intersection Traffic Counts | Matrix | Thursday 25/03/2021 | $6: 00 \mathrm{am}$ to 10:00am <br> $3: 00 \mathrm{pm}$ to 7:00pm |
| Automatic Tube Counts | Matrix | Wednesday 24/03/2021 <br> to Tuesday 30/03/2021 | 24 hours |
| Travel Time Surveys | Matrix | Thursday 25/03/2021 | 6:00am to 10:00am <br> $3: 00 \mathrm{pm}$ to 7:00pm |

### 2.1.1. Annual Average Daily Traffic (AADT)

Annual Average Daily Traffic (AADT) data was assessed for eight permanent traffic collection stations identified within the study area, as presented in Table 2.2 and graphically presented in Figure 2.1.

Table 2.2: Permanent traffic collection stations and locations

| Number | Station ID | Name | Location |
| :--- | :--- | :--- | :--- |
| 1 | 7115 | Canterbury Road | 10m east of King Georges Road, Wiley Park, 2195 |
| 2 | 7275 | Georges River Road | 10m west of Croydon Avenue, Croydon Park, 2133 |
| 3 | 24008 | King Georges Road | 40 m north of The Boulevarde, Wiley Park, 2195 |
| 4 | 24014 | Canterbury Road | 30 m west of Sproule Street, Roselands, 2196 |
| 5 | 24021 | Punchbowl Road | 90 m east of Margaret Street, Belfield, 2191 |
| 6 | 24026 | King Georges Road | 30 north of Roseland Avenue, Roselands, 2196 |
| 7 | 24213 | Canterbury Road | 90 m west of Charles Street, Canterbury, 2193 |
| 8 | 24221 | Bexley Road | 60 m north of South-Western Motorway, Kingsgrove, 2208 |

## EXISTING CONDITIONS

Figure 2.1: Permanent traffic collection stations map


Base map source: Google Maps
AADT data has been utilised to assess the impacts of COVID (if any) and the impacts of seasonality. Detailed analysis has been provided in Section 2.2.

### 2.1.2. Intersection Traffic Counts

Traffic surveys were undertaken on Thursday 25 March 2021 during both the AM and PM peaks, totalling to an eight (8) hour combined period for the following hours:

- 6:00am to 10:00am in the morning peak
- 3:00pm to $7: 00 \mathrm{pm}$ in the afternoon peak.

A total of 34 key intersections within the study area were identified for surveying in consultation with Council and are presented in Figure 2.2.

Intersection counts were used for model calibration.

## EXISTING CONDITIONS

Figure 2.2: Key study intersections


Base map source: Google Maps

### 2.1.3. Automatic Tube Counts

Automatic tube counts (ATC) were collected at 16 sites within the study area to understand the daily and hourly traffic profiles. The locations of these ATC are presented in Figure 2.3. These were used for model calibration.

Figure 2.3: Automatic tube count locations map


Base map source: Google Maps

### 2.1.4. Travel Time Surveys

Travel time surveys (based on a floating car survey) were collected for seven (7) key routes within the study area, presented in Figure 2.4 and outlined in Table 2.3. These were used for base model validation. Travel time route descriptions, locations and the number of runs undertaken across each of the peak periods are outlined below.

Figure 2.4: Travel time survey routes locations


Base map source: Google Maps

## EXISTING CONDITIONS

Table 2.3: Travel time run details

| \# | Route | Direction | Number of Travel Time Runs |  |
| :---: | :---: | :---: | :---: | :---: |
|  |  |  | AM Peak (6:00am 10:00am) | PM Peak (3:00pm 7:00pm) |
| 1 | Lees Avenue (south of Linthorn Avenue), Second Avenue, Ninth Avenue, Loch Street, Evaline Street, Loftus Street, Thorncraft Parade (north of Sunbeam Street) | Northbound | 30 | 29 |
|  |  | Southbound | 30 | 30 |
| 2 | Lees Avenue (south of Linthorn Avenue), Second Avenue, Ninth Avenue, Beamish Street, Bexley Road (north of Cross Street) | Northbound | 38 | 31 |
|  |  | Southbound | 37 | 31 |
| 3 | Brighton Avenue (south of Albert Street), Beamish Street, Bexley Road (north of Cross Street) | Northbound | 28 | 28 |
|  |  | Southbound | 27 | 28 |
| 4 | Brighton Avenue (south of Albert Street), Moore Street, Bellombi Street, Nowra Street, Wairao Street, Wonga Street (north of Canterbury Road) | Northbound | 39 | 39 |
|  |  | Southbound | 39 | 38 |
| 5 | Albert Street (east of Cecilia Street), Ninth Avenue (west of Beamish Street) | Eastbound | 29 | 23 |
|  |  | Westbound | 29 | 23 |
| 6 | Evaline Street (east of Loftus Street, west of Wonga Street) | Eastbound | 28 | 23 |
|  |  | Westbound | 28 | 23 |
| 7 | Canterbury Road (east of Platts Avenue, west of Cooks River crossing) | Eastbound | 25 | 22 |
|  |  | Westbound | 26 | 24 |

### 2.2. Existing Conditions Analysis

### 2.2.1. Annual Average Daily Traffic (AADT)

Permanent traffic counters are located in vicinity of the site area. Two stations were selected to assess the seasonality of traffic volumes, these being:

- $\quad$ Station ID: 24213 - Canterbury Road, 90 metres west of Charles Street
- $\quad$ Station ID: 24014 - Canterbury Road, 30 metres west of Sproule Street.

The selected traffic counters are presented in Figure 2.5 below.

## EXISTING CONDITIONS

Figure 2.5: Selected permanent traffic counter locations


Base map source: Google Maps

Data for year 2018 (for counter 24213) and 2019 (for counter 24014) was analysed to assess the seasonal patterns in this area. Average monthly data is presented in Figure 2.6 and Figure 2.7.

Figure 2.6: Station ID: 24213 - Canterbury Road seasonality analysis


## EXISTING CONDITIONS

Figure 2.7: Station ID: 24014 - Canterbury Road seasonality analysis


As presented in the graphs, March data generally represents averge traffic at both stations on Canterbury Road. Therefore, based on this data, it was considered that March 2021 data would generally represent average traffic conditions and no adjustmens were required to the survey data to account for the seasonality.

### 2.2.2. SCATS Detector Volume Data

SCATS detector count data has been provided for Thursday 21 February 2019, to obtain pre-COVID traffic volumes and to assess the impacts of the COVID-19 pandemic on traffic conditions, if any.

The Beamish Street/ Evaline intersection was selected to conduct comparison of data for AM and PM peak periods.

The comparison of data is shown in Figure 2.8 and Figure 2.9 below.

Figure 2.8: Comparison of AM Peaks - SCATS detector volumes/ intersection counts (8:00am-9:00am)


Figure 2.9: Comparison of PM Peaks - SCATS detector volumes/ intersection counts (5:00pm-6:00pm)


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## EXISTING CONDITIONS

The comparison shows that 2021 data is generally comparable to the 2019 data. Traffic along Evaline Street is higher in 2021 compared to 2019, whereas southbound volumes along Beamish Street are slightly lower. This may be attributed to vehicles using other local roads such as Loch Street, Moore Street, Second Avenue and Wonga Street to access Canterbury Road. Peak directions of travel and general traffic patterns are similar between the two years for the AM and PM peak period.

Therefore, the current survey (2021) data was considered suitable in reflecting existing conditions and was utilised for model development, calibration, and validation.

### 2.2.3. Existing Traffic Volumes

Hourly traffic volumes for the AM and PM peak hours for each of the surveyed intersections is presented in Appendix D.

As expected, a relatively high amount of traffic is observed on the key roads within Campsie such as:

- Canterbury Road - between 3,500 to 4,000 vehicles per hour approaching the intersection of Canterbury Road and Beamish Street.
- Beamish Street - between 1,000 to 1,500 vehicles per hour travelling along the main corridor of Beamish Street between Ninth Avenue and Canterbury Road.
- Ninth Avenue - between 1,000 to 1,500 vehicles per hour travelling along Ninth Avenue, with 1,500 to 2,000 vehicles approaching the intersection with Beamish Street.

Mid-block traffic volumes for a number of road links in the AM and PM peak hours are presented in Figure 2.10 and Figure 2.11 respectively.

## EXISTING CONDITIONS

Figure 2.10: Midblock Traffic Volumes - AM Peak (8:00am-9:00am)


Base map source: Matrix

## EXISTING CONDITIONS

Figure 2.11: Midblock Traffic Volumes - PM Peak (5:00pm-6:00pm)


Base map source: Matrix
Analysis of the existing mid-block traffic counts indicates the following:

- The peak direction of travel during the AM peak period is north-east towards Sydney CBD, with commuters also utilising local roads as well as Beamish Street, Canterbury Road and Brighton Avenue.
- During the PM peak period mid-block flows are generally more distributed, with similar amount of traffic along Canterbury Road and Beamish Street in both directions.
- During the PM peak hour, the peak direction of travel along Brighton Road appears to be southbound towards the Campsie town centre.


### 2.2.4. Existing Speed Profile

Overall average travel times for each of the routes surveyed are presented in Table 2.4.
Table 2.4: Surveyed Travel Time Results - Four Hour Average

| Route <br> ID | Route | Period | Direction | Average Speed <br> $(\mathrm{km} / \mathrm{h})$ | Total Travel Time <br> $(\mathrm{mins})$ |
| :--- | :--- | :--- | :--- | :---: | :---: |
|  | Lees Avenue, Second <br> Avenue, Ninth Avenue, | 6:00am-10:00am | NB | 24 | 7 minutes 14 seconds |
| Route 1Loch Street, Evaline Street, <br> Loftus Street, Thorncraft <br> Parade | 3:00pm-7:00pm | SB | 24 | 7 minutes 8 seconds |  |
|  |  | NB | 24 | 7 minutes 2 seconds |  |
| Route 2 |  | 6:00am -10:00am | NB | 22 | 7 minutes 50 seconds |



In general, the average speed for the key routes varies between $20 \mathrm{~km} / \mathrm{h}$ and $30 \mathrm{~km} / \mathrm{h}$ for both AM and PM peak hours, except for vehicles along Route 2 (Beamish Street) during the PM period. In addition, Route 6 (Evaline Street) has noticeably slower average speeds for eastbound traffic during the PM peak.

Lower average speeds over the entire route are a good indication that the route in its entirety experiences delays (and in turn congestion) and thus these roads are expected to operate close to capacity. To understand which sections are performing at poor levels, level of service was estimated for each section of each of the surveyed routes. This is detailed in the section below.

### 2.2.5. Section Level of Service

The Levels of Service (LOS) of a section of a road can be measured by the average travel speeds along the section. The LOS thresholds as compared to the base Free Flow Speed (FFS) is defined in the Austroads Guide to Traffic Management, Part 3 - Transport Study and Analysis Methods and is provided in Table 2.5.

## EXISTING CONDITIONS

For this analysis, the posted speed limit is assumed to be the base FFS and LOS D (or above) representing the acceptable performance level.

Table 2.5: Section Level of Service Criteria

| Travel speed as a percentage of base <br> Free Flow Speed (FFS) | LOS |
| :---: | :---: |
| $>85$ | A |
| $>67-85$ | B |
| $>50-67$ | C |
| $>40-50$ | D |
| $>30-40$ | E |
| $\leq 30$ | F |

The sections operating close to or at poor levels of service (E or F) for the peak hours are presented in Table 2.6 below.

Table 2.6: Section Performance for Peak Hour- Level of Service

| Route | Direction | Street | End Section | Posted Speed Limit (km/h) | AM (8:00-9:00) |  | PM (5:00-6:00) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Avg. <br> Speed <br> (km/h) | LOS | Avg. <br> Speed <br> (km/h) | LOS |
| 1 | NB | Charlotte Street | Canterbury Road | 50 | 15 | F | 17 | E |
|  |  | Thorncraft Parade | Palmer Street | 50 | 27 | C | 19 | E |
|  |  | Loch Street | Ninth Avenue | 50 | 28 | C | 22 | D |
|  |  | Second Avenue | Seventh Avenue | 50 | 30 | C | 28 | C |
|  |  | Lees Avenue | Linthorn Avenue | 50 | 31 | C | 28 | C |
|  | SB | Second Avenue | Seventh Avenue | 50 | 30 | C | 28 | C |
|  |  | Loch Street | Evaline Street | 50 | 27 | C | 21 | D |
|  |  | Thorncraft Parade | Palmer Street | 50 | 27 | C | 24 | D |
|  |  | Charlotte Street | Canterbury Road | 50 | 16 | E | 21 | D |
|  |  | Charlotte Street | Sunbeam Street | 50 | 30 | C | 30 | C |
| 2 | NB | Bexley Road | Canterbury Road | 60 | 26 | D | 24 | D |
|  |  | Beamish Street | Evaline Street | 50 | 13 | F | 13 | F |
|  |  | Beamish Street | Ninth Avenue | 40 | 25 | C | 23 | C |
|  |  | Ninth Avenue | Fifth Avenue | 40 | 23 | C | 25 | C |
|  |  | Ninth Avenue | Second Avenue | 50 | 20 | D | 12 | F |
|  |  | Second Avenue | Seventh Avenue | 50 | 30 | C | 31 | C |
|  |  | Lees Avenue | Linthorn Avenue | 50 | 30 | C | 30 | C |
|  | SB | Second Avenue | Seventh Avenue | 50 | 31 | C | 30 | C |

## EXISTING CONDITIONS



| Route | Direction | Street | End Section | Posted <br> Speed Limit <br> $(\mathrm{km} / \mathrm{h})$ | AM (8:00-9:00) | PM (5:00-6:00) <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | LOS | Avg. <br> Speed <br> $(\mathrm{km} / \mathrm{h})$ | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | EB | Canterbury Road | Cooks River Crossing | 60 | 24 | E | 35 | C |  |

The results presented in Table 2.6, indicate that:

- Congestion occurs at the key intersections with heavy conflicting flows along both Canterbury Road and Beamish Street.
- Generally, sections along the southern boundary of the study area (connecting to Canterbury Road) and within Beamish Street are expected to operate at capacity (LOS E or F) due to the heavy traffic (1,0001,500 vehicles per hour) estimated along these key roads. This is in line with the observed travel patterns and traffic volumes as presented in Section 2.2.3.
- Based on the average speeds estimated along the sections, the following intersections are expected to be operating at capacity (LOS D or worse) with long delays and queues at some or all approaches:

| $\circ$ | Beamish Street/ Ninth Avenue |
| :--- | :--- |
| 0 | Canterbury Road/ Charlotte Street |
| 0 | Canterbury Road/ Beamish Street/ Bexley Road |
| 0 | Canterbury Road/ Wonga Street |
| 0 | Beamish Street/ Evaline Street |
| 0 | Loch Street/ Ninth Avenue. |

- A number of sections along Beamish Street are generally operating at or close to capacity (LOS E or worse) especially in the PM peak hours.
- Congestion is also observed along Loch Street during the PM peak, with sections operating at LOS E.


## 3. MODEL ASSUMPTIONS



### 3.1. Modelling Platform

The model was developed using Aimsun Next version 20.0.2.

### 3.2. Network

The base network was developed with an import of OSM with reference to the major connections in the Sydney Travel Forecasting Model (STFM) base model network. Additional connections were introduced where appropriate to produce a more refined network and zoning structure. The network geometry was coded with reference to Google Maps and NearMap aerial photography to ensure the network was represented accurately.

### 3.3. Time Period

A two-hour period was modelled as part of this study for both the AM and PM peak periods with 30-minute warm-up and 30-minute cool-down periods, created by profiling the peak period demands. Table 3.1 lists the modelled peak times

Table 3.1: Modelled Time Periods

| Peak | Warm-up times | Model Period | Cool Down |
| :---: | :---: | :---: | :---: |
| AM Peak | $6: 45 \mathrm{am}-7: 15 \mathrm{am}$ | $7: 15 \mathrm{am}-9: 15 \mathrm{am}$ | $9: 15 \mathrm{am}-9: 45 \mathrm{am}$ |
| PM Peak | $2: 45 \mathrm{pm}-3: 15 \mathrm{pm}$ | $3: 15 \mathrm{pm}-5: 15 \mathrm{pm}$ | $5: 15 \mathrm{pm}-5: 45 \mathrm{pm}$ |

### 3.4. Vehicle Types

Two vehicle types were adopted: light vehicles (LV) and heavy vehicles (HV). Matrices for both vehicle types were developed and calibrated separately.

### 3.5. Traffic Zones

The model zoning system comprises 97 travel zones, shown graphically in Figure 3.1. All external zones are numbered 1 to 15 , and all internal zones are named with the corresponding STFM zone followed by a letter system.

Figure 3.1: Aimsun Model Zones


### 3.6. Road Types

Roads were coded to match the existing road network and intersection geometry including the correct configuration, lane designation and permitted turning movements. U- turns were permitted and coded at roundabouts. The modelled road hierarchy is presented in Figure 3.2.

Figure 3.2: Modelled Road Types


### 3.7. Speed Profiles

Sign posted speed limits were used throughout the model and this is presented in Figure 3.3. A majority of the network is $50 \mathrm{~km} / \mathrm{h}$, with the only exceptions being Canterbury Road ( $60 \mathrm{~km} / \mathrm{h}$ ) and Beamish Street through Campsie town centre ( $40 \mathrm{~km} / \mathrm{h}$ ).

Figure 3.3: Modelled Speeds


### 3.8. School Zones

There are three school zones within the study area that are restricted to $40 \mathrm{~km} / \mathrm{h}$ speed limits during school time periods. The schools are:

1. Harcourt Public School
2. Wangee Park School
3. Campsie Public School.

The $40 \mathrm{~km} / \mathrm{h}$ speed zones are presented in Figure 3.4 and were only implemented during the school hours of 8:00am to 9:30am and 2:30pm to 4:00pm.

Figure 3.4: School Zones within the Study Area


### 3.9. Traffic Signals

### 3.9.1. SCATS

Traffic signal characteristics for the base year model were derived from an extensive analysis of SCATS data. All intersections and interchanges within the model cordon were developed with actuated control. The signal groups and the associated detector functionalities and phasing specifications were all estimated from analysis and interrogation of provided traffic signal control plans and historic signal timings (SCATS data).

Minimum and maximum green times for each signal phase were calculated in one-hour intervals for each intersection in the corresponding modelled period. Phase sequences, signal offsets and special conditions were incorporated as relevant to existing SCATS operations.

The linking of intersections can vary throughout the day within SCATS; however, it is typical that Link Plan 4 operates during the AM peak while Link Plan 2 operates during the PM peak. Analysis of the SCATS LX data outlined that the signalised intersections are coordinated along Canterbury Road and along Beamish Street. Offsets have been applied to the model accordingly.

It is noted that some adjustments were made to the signal timing to account for pedestrian movements. As pedestrians were excluded from the model, the green times for pedestrian affected movements were adjusted based on expected delays and approximate call frequency rate of the signalised crossing.

### 3.9.2. Canterbury Road End Constraints

Travel times and congestion along Canterbury Road indicated significant congestion originates outside of the study area. The congestion on Canterbury Road in the eastbound direction can be seen to originate to the east of Cooks River Crossing, at the Broughton Street intersection. This is shown graphically by the Google Maps estimated traffic tool in Figure 3.5.

Figure 3.5: Google Maps Congestion at Cooks River Crossing (AM Peak)


In order to replicate this in the base model, the signal data for the signalised intersections either side of Canterbury Road study area boundaries were analysed. Metering was included in the model at both ends of Canterbury Road to replicate the average green times applied to the movements exiting the model. It is noted that due to the actuated control of these intersections, the average green times required slight adjustment in the validation process.

### 3.10. Traffic Management

The Campsie model study area includes a large number of routes with traffic calming devices (speed bumps). Locations of speed bumps in the study area are outlined in Figure 3.6.

Figure 3.6: Speed Bump Locations within the study area


In addition to the above locations, there are a number of locations, particularly along Beamish Street with high pedestrian activity and friction caused by on-street parking (parallel parking). For all these locations, appropriate speed reductions have been developed to reflect the reduced speeds occurring due to the combination of all of these factors. These speed reductions have been coded as traffic management plans within Aimsun and have been applied directly to the Stochastic Route Choice assignments, as it is deemed due to the extensive reach of these speed reductions across the study area that they will not influence route choice.

### 3.11. Public Transport

All public transport lines and schedules are coded as fixed routes as per the latest timetables available from the open source General Transit Feed Specification (GTFS) data.

A map of the public transport routes and services included in the model is shown in Figure 3.7.

Figure 3.7: Public Transport Map


Base image source: Transit Systems Inner West Network Map

### 3.12. Demand Development

Six key steps were undertaken during the development of the demand matrices as outlined in Figure 3.8.

Figure 3.8: Base Model Demand Development Procedure


1. Cordon Matrices from STFM - cordon matrices were extracted from the STFM provided for the study area as outlined in the Campsie Stage 1 Analysis report, 17/03/2021. These matrices provide the initial OD structure at the Travel Zone level.
2. Zone Splitting - travel zones were further disaggregated into a more detailed structure for the additional detail required for the mesoscopic model. Mesh block data are a refined subset of SA1 data sets and are the 'building blocks' of the census data. 2016 mesh block data has been used to determine the proportion of trips being attracted and generated by each of the zones within each travel zone to proportion the demand obtained from step 1 to the new zone structure. It is noted that each mesh block has been assigned to a centroid only within the corresponding STFM zones. QGIS was used to initially analyse this data and provide a platform to appropriately match geographic locations and zones. A screenshot of this analysis can be seen in Figure 3.9 below.

Figure 3.9: QGIS mesh block analysis for STFM to Aimsun zone disaggregation

3. Matrix Finessing - the survey data was utilised to determine the known origin and destination totals and the OD pair totals. The matrices developed in step 2 were refined (finessed) to match the totals while maintaining the structure of the matrix.
4. Static Adjustment - the matrices from step 3 were then imported into Aimsun where the static adjustment tool was used to further refine the matrix to represent survey data.
5. Departure Adjustment - a departure adjustment scenario was undertaken in Aimsun to determine the 15-minute demand profile.
6. Manual Adjustments - some minor additional manual adjustments were undertaken to better reflect observed counts and congestion in the network. Only two manual adjustments were made, with both in the PM peak demands, where initial assumptions on the zone split around Beamish Street in Campsie town centre needed refinement.

The resultant demand profiles for the normal weekday AM and PM peak periods are presented in Figure 3.10 and Figure 3.11 while a comparison of the trip length distribution between the prior and the adjusted matrix is shown in Figure 3.12, Figure 3.13, Figure 3.14 and Figure 3.15 for the AM and PM peaks respectively.

Figure 3.10:Traffic Demand Profile AM Peak


Figure 3.11:Traffic Demand Profile PM Peak


Figure 3.12: Trip Length Distribution - AM Peak (7:30am - 8:30am)


Figure 3.14: Trip Length Distribution - PM Peak (4:15pm - 5:15pm)


Figure 3.13: Trip Length Distribution - AM Peak (8:30am - 9:30am)


Figure 3.15: Trip Length Distribution - PM Peak (5:15pm - 6:15pm)


The trip distribution figures show that minimal changes have been made in the overall distribution from the STFM estimated prior matrices and the adjusted demands estimated with the static adjustment experiments for both hours of the AM and PM peaks.

### 3.13. Assignment

Two assignment types within the Aimsun software package were adopted to inform and develop the base year model demands. The static (macro) and dynamic (mesoscopic) assignment types are discussed below to indicate their purpose in the assessment.

### 3.13.1.Static Assignment

Prior to running the dynamic scenario, a static assignment experiment was run to generate an initial path assignment file (APA file) for use as a starting point for the dynamic scenario. This provides a suitable base with available paths from which the vehicles in the dynamic scenario will follow. An industry accepted check of the paths generated in the static assignment was undertaken by utilising the select link analysis and path assignment tools, pinpointing reasons for the unrealistic paths or bad matches between the survey and the modelled results. To ensure unrealistic paths were eliminated, Volume Delay Functions (VDF) were refined and applied with one set VDF for each road type. The VDF refinements incorporated adjusted factors based on both section speed and section capacity to ensure similar route choices were made between STFM (as per select link analysis outputs) and the Aimsun Mesoscopic Base Model.

### 3.13.2.Dynamic User Equilibrium Route Choice Assignment

Dynamic User Equilibrium (DUE) traffic assignment within the Aimsun models was used to run the dynamic scenarios. This is considered the most appropriate method given the scope of the road network model and potential future alternate routes that may alter travel patterns.

The DUE assignment is an iterative process where vehicles are released into the model network, select a preferred route, and respond to the cost of their route choice (as a function of travel time and delay) as a result of traffic conditions within the model, changing its route if deemed appropriate. This provides a realistic representation of the actual driver behaviour where drivers have their own perception on when to make the decision and change their route and avoid delays.

The DUE assignment runs over a number of iterations (predetermined maximum) until it reaches the maximum, or a state of equilibrium or convergence measured as the relative gap in the path costs for each path assignment cycle ( 15 minutes). Achieving convergence before the maximum iterations is exhausted indicates that the travel behaviour in the network between the previous and current iteration is able to be closely replicated for the entire simulation period, therefore suggesting the model is in a stable condition and suitable for assessment.

During the model development process, the following process was undertaken to ensure that the demands were suitable for each of peak period simulations:

- Each DUE assignment was assessed in terms of relative gap, regression slope, number of vehicles waiting to enter, number of vehicles in the network and the number of vehicles that went through.
- Validity of the DUE paths were assessed to ensure unrealistic paths were not being assigned between any origin-destination pairs.


### 3.14. Dynamic Cost Function

The dynamic cost function for the meso model was adjusted from the default cost function provided within the Aimsun software. This was undertaken to not only consider travel time as a cost but also distance travelled. A comparison of the two functions is shown below:

## Default Cost Function

Dynamic Cost $=$ TT + TT $\times$ AW $\times$ A + UDCW * UDC

## Adjusted Cost Function

Dynamic Cost $=\mathrm{TT}+\mathrm{TT} \times \mathrm{AW} \times \mathrm{A}+\mathrm{UDCW} \times \mathrm{UDC}+\mathrm{D} \times \mathrm{DW}$
Where:
TT = Estimated Travel Time
A = Attractiveness
AW = Attractiveness Weight
UDC = User Defined Cost
UDCW = User Defined Cost Weight
D = Distance
DW = Distance Weight

Further, the methodology used to calculate the attractiveness weight of each link was adjusted to reflect attractiveness as a function of road type and not overall capacity. This was adjusted as the default methodology applies greater differences to the attractiveness weighting for higher order roads and less of an impact for lower order roads. This does not reflect overall route choice in which vehicles will typically choose higher order roads based on travel time of total journey with local roads used typically used to access the desired destination.

### 3.15. Behaviour Parameters

Table 3.2 provides a summary of all global model parameters used to simulate the existing conditions and outlines any departures from the default values.

Table 3.2: Global Parameters

| Parameters | Default Value | Model Value |
| :--- | :---: | :---: |
| Reaction Time | 1.2 | 1.2 |
| Reaction Time at Traffic Light | 1.6 | 1.6 |
| DUE Model | Gradient Based | Gradient Based |
| Maximum Iterations | 20 | 20 |
| Relative Gap | $0.5 \%$ | $0.5 \%$ |
| Arrivals | Exponential | Uniform |
| Attractiveness Weight | 0 | 4 |
| User Defined Cost Weight | 0 | 0 |

Any changes to these global parameters were made to better reflect the current behaviour of the transport system as part of the standard model calibration process.

### 3.15.1.Vehicle Parameters

Default vehicle parameters were adopted for the model except for the changes outlined in Table 3.3.
Table 3.3: Vehicle Parameters

| Parameters | Car |  | Truck |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Default Value | Model Value | Default Value | Model Value |  |
| Speed Limit <br> Acceptance | Mean | 1.10 | 0.85 | 1.05 | 0.85 |
|  | Deviation | 0.10 | 0.10 | 0.10 | 0.10 |
|  | Minimum | 0.90 | 0.75 | 1.00 | 0.75 |
|  | Maximum | 1.30 | 0.95 | 1.10 | 0.95 |

The travel time data analysis generally indicated that vehicles within the study area adhere to posed speed limits. This is further enforced by presence of multiple speed cameras and red-light cameras along key routes and intersections within the LGA. Therefore, the Speed Limit Acceptance was reduced from the default values to ensure all simulated vehicles will travel below the posted speed limits.

### 3.16. Calibration and Validation criteria

The base model was calibrated and validated in accordance with TfNSW 'Traffic Modelling Guidelines 2013'. Table 3.4 presents the relevant targets:

Table 3.4: Adopted Calibration and Validation Criteria

| Item | Criteria |
| :---: | :---: |
| Turn Volumes | Tolerance limits for turn volumes: <br> - GEH $\leq 5$ for at least $85 \%$ of link flows <br> - GEH $\leq 5$ for at least $85 \%$ of turn flows <br> - All Link and turn flows should have $\mathrm{GEH} \leq 10$ <br> - $\quad R^{2}$ value for Observed vs. Modelled plots to be $>0.9$. |
| Travel Time Average | - Average modelled journey time to be within $15 \%$ or one minute (whichever is greater) of average observed journey time for full length of route. <br> - Average modelled journey time to be within $15 \%$ of average observed journey time for individual sections. |
| Model Stability | - Model convergence should be achieved. Parameters for convergence have been adopted from the Transport for London traffic modelling guidelines and consist of the following. <br> - $95 \%$ of all path volumes change by less than $5 \%$ for at least four (4) consecutive iterations. <br> - $95 \%$ of travel times on all paths change by less than $20 \%$ for at least four (4) consecutive iterations. |

Full details of the model calibration and validation process are included in Appendix $\mathrm{A}, \mathrm{B}$ and C .

## 4. FUTURE YEAR MODELS



### 4.1. Future Year Scenarios

As discussed in the Stage 1 modelling report, an alternative route, west of Campsie Town Centre (Option 1), is being considered to provide an alternative north-south connection between Canterbury Road and Georges River Road. Option 1 is also expected to alleviate some congestion from Beamish Street, providing opportunities for land use uplift within the Campsie Town Centre.

To test the potential impacts and benefits of the proposal, it is also necessary to develop a suitable baseline in which to compare the results. To this end, the existing road network conditions have been modelled under the following future year scenarios for both the AM and PM peak periods to enable appropriate comparisons:

```
- 2026 Future Base (Do Minimum)
O 2036 Future Base (Do Minimum).
```

The Future Base (Do Minimum) model results are discussed within this section of the report, whilst the Option Testing is discussed in Section 5.

### 4.2. Future Year Demand

### 4.2.1. Methodology

The future year demands have been obtained from the strategic modelling undertaken and discussed within the Stage 1 modelling report. The future STFM scenarios considered various future infrastructure changes that have impacted the study area future demands; however, the zone structure for the study area itself have remained consistent between base and Future Do Minimum scenarios. The following process summarises the steps undertaken in order to develop Future Do Minimum Aimsun model demands:

1. Using a cordon to represent the Masterplan Area in the Stage 1 STFM model, calculate 2-hour OD demand differences between Base and Future Do Minimum STFM scenarios (i.e., STFM 2026 AM Peak - STFM 2019 AM Peak).
2. Absolute demand differences were then applied to each Aimsun 15-minute matrix, by vehicle type, based on the proportion of those demands for the corresponding overall STFM zone.
3. Warm-up and cool-down matrices were given the same proportions to the first and last 15-minute matrix as was done for the base models.

### 4.2.2. Demand Summary

The following table outlines the 2-hour total demands applied in the Aimsun mesoscopic models. These include traffic travelling through the study area as well as traffic travelling within the study area.

Table 4.1: 2-hour Aimsun Total Demands - Future Base

| Peak | 2021 (Base) | 2026 |  | 2036 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Demand | Demand | Growth (p.a.) | Demand | Growth (p.a.) |
| AM Peak | 22,741 | 25,361 | $2.3 \%$ | 27,508 | $0.8 \%$ |
| PM Peak | 25,862 | 28,756 | $2.2 \%$ | 31,104 | $0.8 \%$ |

### 4.3. Future Do Minimum Model Assumptions

### 4.3.1. Road Network

For the future do minimum models, the road network, including all intersection configuration, method of control, speed limits, traffic management measures (i.e., speed bumps) have remained exactly as per the base year base model. The only exception to this is for the future PM models which experienced issues in the mesoscopic scenarios at the Ninth Avenue, Loch Street and Second Avenue roundabouts. In a number of the SRC experiments, this area caused unrealistic network-wide gridlock. The base model traffic management plan at this location had originally been carried through to the Future Do Minimum PM scenarios, with the school zone speed limit ( $40 \mathrm{~km} / \mathrm{h}$ ) further reduced to $30 \mathrm{~km} / \mathrm{h}$ due to speed bumps. It was determined that this particular traffic management plan was the cause of the gridlock issues. For the purposes of this assessment, this traffic management plan was altered back to the school zone posted speed limit of $40 \mathrm{~km} / \mathrm{h}$. This was applied for both the Future Do Minimum 2026/2036 PM scenario and the Future Option 2026/2036 PM scenarios.

### 4.3.2. Traffic Signal Timing

For the future do minimum modelling, some minor changes have been permitted to the control plans developed for the signalised intersections to accommodate changes in demands. The changes made to the control plans have altered the minimum and maximum phase time permitted to operate for various approaches. These changes have been limited to the Canterbury Road, Beamish Street and Bexley Road intersection, which is a major cause of congestion for the study area both north-south and east-west and required some optimisation for various movements.

It is also noted that the base model end constraints applied at either end of Canterbury Road, to replicate exterior congestion issues, have been maintained in the Future Do Minimum model scenarios.

### 4.4. Future Do Minimum Model Results

### 4.4.1. Overview

The following sections outline the expected level of performance under the 2026 and 2036 Future Do Minimum model scenarios in comparison to the 2021 Base year model results. Analysis includes the following:

1. Network Performance

- overall performance
- density plots.

2. Travel Times

All scenarios have been run with 5 seeds as per the calibrated and validated base models, with the outputs reported for the median seed of each.

## FUTURE YEAR MODELS

### 4.4.2. Overall Network Performance

The following network performance statistics have been reported on for comparative purposes:

- Vehicle Kilometres Travelled - VKT (km) represents the total travelled distance of all vehicles during the simulation period.
- Vehicle Hours Travelled - VHT (h) represents the total travel time of all vehicles during the simulation period.
- Average Speed (km/h) represents the average speed of all vehicles during the simulation period (VKT/ VHT).
- Delay (sec/km) represents the average delay of all vehicles during simulation period per unit distance (sec/km).
- Latent Demand (vehicles) represents the unreleased demand into the network at the end of the simulation period.

A summary of the network performance of the existing road network under the future 2026 demands in comparison to the base 2021 as well as 2036 demands in comparison to 2026 is presented in Table 4.2.

Table 4.2: Future Base - Do Minimum Network Performance Statistics

| Peak Period | Time | Network Statistic | Base | Future Do Minimum |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2021 | 2026 | 2036 |
| AM Peak | $\begin{aligned} & \text { 7:30am- } \\ & \text { 8:30am } \end{aligned}$ | VKT (km) | 19,211 | 20,911 | 21,623 |
|  |  |  |  | 8.8\% | 3.4\% |
|  |  | VHT (h) | 809 | 1,097 | 1,191 |
|  |  |  |  | 35.6\% | 8.6\% |
|  |  | Average Speed (km/h) | 27.1 | 25.0 | 24.9 |
|  |  |  |  | -7.7\% | -0.6\% |
|  |  | Delay (sec/km) | 63 | 95 | 103 |
|  |  |  |  | 50.5\% | 9.0\% |
|  | $\begin{aligned} & \text { 8:30am- } \\ & \text { 9:30am } \end{aligned}$ | VKT (km) | 19,424 | 21,175 | 22,043 |
|  |  |  |  | 9.0\% | 4.1\% |
|  |  | VHT (h) | 773 | 1,181 | 1,330 |
|  |  |  |  | 52.8\% | 12.6\% |
|  |  | Average Speed (km/h) | 28.1 | 24.1 | 23.6 |
|  |  |  |  | -14.3\% | -2.1\% |
|  |  | Delay (sec/km) | 54 | 104 | 122 |
|  |  |  |  | 93.6\% | 16.5\% |
|  |  | Latent Demand (veh) | 1 | 502 | 1,153 |
|  |  |  |  | 50100\% | 130\% |
| PM Peak | $\begin{aligned} & \text { 4:15pm- } \\ & 5: 15 \mathrm{pm} \end{aligned}$ | VKT (km) | 21,630 | 23,551 | 25,064 |
|  |  |  |  | 8.9\% | 6.4\% |


| Peak <br> Period | Time | Network Statistic | Base | Future Do Minimum |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2021 | 2026 | 2036 |
|  |  | VHT (h) | 855 | 945 | 1,111 |
|  |  |  |  | 10.5\% | 17.6\% |
|  |  | Average Speed (km/h) | 28.1 | 27.8 | 26.2 |
|  |  |  |  | -1.2\% | -5.7\% |
|  |  | Delay (sec/km) | 54 | 56 | 70 |
|  |  |  |  | 5.1\% | 23.4\% |
|  | $\begin{aligned} & \text { 5:15pm- } \\ & 6: 15 \mathrm{pm} \end{aligned}$ | VKT (km) | 21,815 | 23,656 | 25,169 |
|  |  |  |  | 8.4\% | 6.4\% |
|  |  | VHT (h) | 862 | 1,089 | 1,409 |
|  |  |  |  | 26.4\% | 29.3\% |
|  |  | Average Speed (km/h) | 27.9 | 25.6 | 23.5 |
|  |  |  |  | -8.2\% | -8.4\% |
|  |  | Delay (sec/km) | 54 | 76 | 108 |
|  |  |  |  | 40.1\% | 42.5\% |
|  |  | Latent Demand (veh) | 1 | 1 | 23 |
|  |  |  |  | 0\% | 2200\% |

The following key outcomes are noted with regards to the overall network statistics:

- AM Peak:
- Across the overall road network, VKT and VHT have increased in 2026 and 2036 Do Minimum scenarios. This is predominantly due to the increased demand.
- Average speeds for all vehicles across the entire network can also be expected to reduce by 7$15 \%$ in 2026 and reduce by a further $2 \%$ in 2036.
- Latent demand significantly increases in both 2026 and 2036, with the expected total latent demand in 2036 representing approximately $4 \%$ of the overall demand. This is mostly due to the excessive queueing on Canterbury Road.
- The overall network is seen to perform worse in the second hour of the AM Peak period than the first hour.
- PM Peak:
- Similar overall performance patterns are observed in the PM peak as in the AM peak.
- VKT and VHT increase significantly in both 2026 and 2036, corresponding to a reduction in overall network speeds of up to $9 \%$.
- With no significant queueing on Canterbury Road, the PM peak experiences minimal latent demand.
- As was noted in the AM peak, the second hour of the PM peak is worse than the first.


### 4.4.3. Route Performance (Travel Times)

Average total travel times for each of the routes modelled are presented in Figure 4.1 to Figure 4.4 below, with base model travel times included for comparison.

Figure 4.1: Average Travel Times (sec) - AM Peak (7:30am-8:30am)


Figure 4.2: Average Travel Times (sec) - AM Peak (8:30am-9:30am)


Figure 4.3: Average Travel Times (sec) - PM Peak (4:15pm-5:15pm)


Figure 4.4: Average Travel Times (sec) - PM Peak (5:15pm-6:15pm)


## FUTURE YEAR MODELS

The network travel times indicate an increase in delays across the network for both 2026 and 2036 Do Minimum scenarios. The following key observations are made for the AM and PM peaks respectively:

- AM Peak:
- The most significant increase in travel times is observed on Canterbury Road (Route 7), particularly from the base year to 2026 Do Minimum scenario.
- Increases in travel times are also noted for Route 2 and Route 3, which are attributed to the increased demand and corresponding delays both northbound and southbound on Beamish Street.
- $\quad$ This is significantly worse for the northbound direction of both Routes 2 and 3.
- As noted with the overall network statistics, travel times are worse in the second AM peak hour than the first hour.
- PM Peak:
- The PM peak future base models operate similarly to the AM peak, with no major increases in network route travel times with the exception again of Routes 2,3 and 7 .
- Route 7 is seen to increase in both PM peak hours across all years, though not as drastically as the AM peak as there are less significant capacity end constraints in the PM peak on Canterbury Road.
- Route 2 and Route 3 experience large increases in overall route travel time, particularly for the northbound direction, with overall travel times increasing by over 100\% in the second PM Peak hour from the Base model to the 2036 Do Minimum model scenario.


### 4.4.4. Network Congestion

The following section highlights the overall network simulated density, which pinpoints critical locations causing congestion. Figure 4.5 and Figure 4.6 include model simulated density plots for the AM and PM peaks respectively.

Figure 4.5: Aimsun Base and Future Base Model Simulated Density - AM Peak (9:00am)


The results of the simulated density plots analysis in the AM peak generally indicate the following:

- Major congestion build up is observed on the following corridors:
- Canterbury Road both eastbound and westbound (worse in eastbound peak direction)
- Ninth Avenue at the Loch Street roundabouts
- the southern end of Beamish Street both northbound and southbound due to delays caused by the signals at both Canterbury Road and Evaline Street.
- Route diversion is observed for Canterbury Road eastbound, with vehicles travelling northbound at Tudor Street and Thorncraft Parade off Canterbury Road due to the significant delays from the external signals. There is also expected diversions for vehicles that would travel northbound at Beamish Street from Canterbury Road that divert due to the Beamish Street northbound congestion issues.
- Both Canterbury Road and Beamish Street corridors are significantly more congested in 2026 and 2036 Do Minimum scenarios.

Figure 4.6: Aimsun Base and Future Base Model Simulated Density - PM Peak (6:15pm)


The results of the simulated density plots analysis in the PM peak generally indicate the following:

- Congestion locations in the PM peak scenarios remained relatively consistent across design years, with larger congestion and a significant breakdown in flow seen by the 2036 Do Minimum scenario within a number of key corridors.
- Major congestion is observed at the following locations:
- Canterbury Road due to the interactions and operation of the Beamish Street and Bexley Road intersection
- Beamish Street northbound and southbound between Evaline Street and Canterbury Road, as well as the south approach to Canterbury Road
- Ninth Avenue east approach to the Loch Street roundabouts as well as the linked Fifth Avenue corridor both northbound and southbound.


## 5. OPTIONS SCENARIO MODELS



### 5.1. Overview

As discussed in the Stage 1 modelling report, an alternative route, west of Campsie Town Centre (Option 1), is being considered to provide an alternative north-south connection between Canterbury Road and Georges River Road. Option 1 is also expected to alleviate some congestion from Beamish Street, providing opportunities for land use uplift within the Campsie Town Centre. The proposed layout for Option 1 is presented in Figure 5.1.

Figure 5.1: Proposed West Campsie Alternative Route


### 5.2. Future Year Option Model Assumptions

### 5.2.1. Future Option Demands

Demand for the options model scenarios was developed with the same methodology as was applied for future base models; with the exception that the absolute differences were calculated between future base and options STFM matrices as opposed to base year and future base scenarios. It is noted in a number of instances, the future options scenarios have less demand to/from zones than the future base scenarios due to the introduction of the bypass.

Table 5.1: 2-hour Aimsun Total Demands - Future Option Scenarios

| Peak | Year | Base | Bypass | Abs. Difference |
| :---: | :---: | :---: | :---: | :---: |
| AM Peak | 2021 | 22,741 | - | - |
|  | 2026 | 25,361 | 26,003 | 642 |
|  | 2036 | 27,508 | 27,879 | 371 |
| PM Peak | 2021 | 2026 | 28,756 | - |

The overall 2-hour mesoscopic Aimsun demands remain relatively consistent between the Base and corresponding Bypass scenarios, with the Bypass options scenarios yielding slightly greater total demands in the order of 350-800 vehicles. This is likely a result of the increased attractiveness in the strategic model due to the introduction of the bypass.

### 5.2.2. Road Network

For the future year options models, the majority of the road network, including all existing intersection configuration, method of control, speed limits, traffic management measures (speed bumps) have remained consistent with the Base and Future Do Minimum models.

The notable exception is along the proposed alternative route, where the model has been updated to include:

- Removing speed bumps and chicanes along the bypass route.
- Upgrading the full bypass route to road type "Undivided Sub-Arterial" to match that of Beamish Street.
- Providing direct connection between Second Avenue, Loch Street, Orissa Street and Viking Street.

The assumed intersection configuration and control at the new connections are shown in Figure 5.2 to Figure 5.5.

The main changes are noted as follows:

- Canterbury Road / Viking Street / Orissa Street - realign the Viking Street and Orissa Street to provide a signalised cross intersection rather than the existing staggered t-intersections.
- Evaline Street - create a new south approach which joins Orissa Street to Loch Street. Convert the existing roundabout to a signalised cross intersection.
- Ninth Avenue - realign the north approach to align with the south approach and provide a signalised cross intersection rather than the existing staggered roundabout t-intersections.
- Second Avenue / Seventh Avenue - convert the existing roundabout to a signalised cross intersection.

Figure 5.2: Canterbury Road Configuration


Figure 5.4: Ninth Avenue Configuration


Figure 5.5: Seventh Avenue Configuration


Other minor adjustments were made to intersections along the bypass corridor to ensure appropriate priority was provided to the bypass movements. This included removal of the roundabout at Campsie Street and Loch Street and reducing the attractiveness for east-west movements along Claremont and Fletcher Street to reduce the amount of rat-running between the Bypass and surrounding higher order roads.

### 5.2.3. Traffic Signal Timing

To inform the optimal operation of the proposed signalised intersections along the bypass, intersection models were developed using SIDRA Intersection. These models used the anticipated demands, a minimal geometry and typical intersection phasing in order to determine how the minimal intersection layout configurations would operate. An iterative process was then undertaken following interrogation of the anticipated turning demands to identify if additional lanes or alternative phasing arrangements resulted in better performance.

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The resultant intersection configurations are shown in Figure 5.6 to Figure 5.9 and their high-level SIDRA results are shown Table 5.2.

Figure 5.6: Canterbury Road Configuration


Figure 5.8: Ninth Avenue Configuration


Figure 5.7: Evaline Street Configuration


Figure 5.9: Seventh Avenue Configuration


Table 5.2: Preliminary SIDRA Results for Signalised intersections - Future Option Scenarios

| Location | AM Peak |  | PM Peak |  |
| :--- | :---: | :---: | :---: | :---: |
|  | DOS | LOS | DOS | LOS |
| Bypass and Canterbury Road (2036) | 0.97 | E | 1.00 | E |
| Bypass and Evaline Street (2036) | 0.85 | C | 0.86 | C |
| Bypass and Ninth Avenue (2036) | 0.90 | C | 0.92 | D |
| Bypass and Seventh Avenue (2036) | 0.82 | C | 0.92 | D |

The results suggest that the proposed intersection configurations have the potential to operate satisfactorily in the future, with the exception of the Canterbury Road / Bypass intersection which would be at capacity. However, it is noted that Canterbury Road is already approaching capacity and therefore this would be a function of the anticipated demands, not because of the proposed intersection changes.

Once satisfactory performance of the intersection was achieved for the 2036 scenarios in SIDRA, the intersection geometry and phasing in the AIMSUN model was updated. The traffic signal phase splits identified in the SIDRA models were used as the basis of the actuated signal plans noting that:

- Minimum phase times were set to be 12 seconds, with 6 seconds green, 4 seconds yellow and 2 seconds all red.
- Maximum phase times were set to have at least 6 seconds more green time than calculated by SIDRA.


### 5.3. Future Option Model Results

### 5.3.1. Overview

The following section compares all Future Do Minimum scenarios with the corresponding Future Bypass scenarios, with the results taken from the median seed run for each. As was outlined in the Future Do Minimum analysis, this section highlighted performance based on network statistics, travel times, overall network congestion and a review of demand changes due to the implementation of the bypass.

### 5.3.2. Overall Network Performance

A summary of the network performance of the Bypass options in comparison to the Future Do Minimum scenarios with both 2026 and 2036 demands is presented in Figure 5.2.

Table 5.3: Future Year - Option Network Performance Statistics

| Peak Period | Time | Network Statistic | 2026 |  | 2036 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Base | Bypass | Base | Bypass |
| AM Peak | $\begin{aligned} & \text { 7:30am- } \\ & \text { 8:30am } \end{aligned}$ | VKT (km) | 20,911 | 21,505 | 21,623 | 22,337 |
|  |  |  |  | 2.8\% |  | 3.3\% |
|  |  | VHT (h) | 1,097 | 1,146 | 1,191 | 1,243 |
|  |  |  |  | 4.5\% |  | 4.4\% |



The following key outcomes are noted with regards to the overall network statistics:

- AM Peak:
- Across the overall road network, VKT and VHT have increased in 2026 and 2036 Bypass scenarios in comparison to the Future Do Minimum scenarios. This is due to both the increase in overall demand and the introduction of several signalised intersections as part of the bypass supporting infrastructure.
- Average speeds for all vehicles across the entire network can also be expected to reduce by up to $1.6 \%$ with the bypass in 2026 and reduce by a further $2.5 \%$ in 2036.
- Latent demand decreases in both 2026 and 2036 Bypass scenarios by an estimated $12.5 \%$ and $16.7 \%$ respectively.
- The overall network is seen to perform similarly in both the first and second AM peak hours.
- PM Peak:
- Similar overall performance patterns are observed in the PM peak as in the AM peak.
- VKT and VHT increase in both the 2026 and 2036 Bypass scenarios, corresponding to a reduction in overall network speeds of up to $5 \%$.
- The PM peak scenarios all experience minimal latent demand.
- A more significant drop in overall performance is noted in the 2026 PM scenarios compared to the 2036 scenarios.
- The second hour of the PM peak is observed to operate slightly worse than the first hour, with more significant drops in average speeds and increases in overall network delays.

Figure 5.10 to Figure 5.13 include comparisons of overall network speeds and the corresponding throughput for each hour of the peak periods for the Future Do Minimum and Bypass scenarios.

Figure 5.10:Total Throughput and Network Speeds - AM Peak (7:30am-8:30am)


Figure 5.11:Total Throughput and Network Speeds - AM Peak (8:30am-9:30am)


Figure 5.12:Total Throughput and Network Speeds - PM Peak (4:15pm-5:15pm)


Figure 5.13:Total Throughput and Network Speeds - PM Peak (5:15pm-6:15pm)


The results show that the introduction of the bypass increases the network throughput (capacity) in all peak periods and scenarios when compared to the base. The drop in average speed corresponds with the introduction of signalised intersections which are needed to support the bypass.

### 5.3.3. Route Performance (Travel Times)

A comparison of overall modelled travel time routes between Future Do Minimum and Bypass option scenarios is included below in Figure 5.14 to Figure 5.17.

Figure 5.14:Average Travel Times (sec) - AM Peak (7:30am-8:30am)


Figure 5.15:Average Travel Times (sec) - AM Peak (8:30am-9:30am)


The AM peak period travel time results indicate the following:

- Some disbenefits are observed for Canterbury Road (Route 7), with travel times increasing slightly in both hours of the 2026 models. The eastbound travel times in the 2036 Bypass option seen to balance across the 2-hour peak, with some increases in travel times in the first hour and decreases in the second hour (likely due to an increased throughput able to make it through in the first hour), with less friction at the Beamish Street and Bexley Road intersection.
- The east-west connections on Evaline Street and Ninth Avenue (Route 5 and 6) also experience increased overall travel times due to the increase in the competing bypass demands and the corresponding priority and coordination provided for the north-south movement.
- Significant benefits in travel time savings, particularly in the second hour of the models, are noted for Route 2 and 3 which correlates to the reduction in demand both northbound and southbound on Beamish Street through Campsie town centre. The peak travel time savings for this route are observed
in the second hour of the 2036 scenarios, with reductions of approximately $60 \%$ for Route 3 northbound.

Figure 5.16:Average Travel Times (sec) - PM Peak (4:15pm-5:15pm)


Figure 5.17:Average Travel Times (sec) - PM Peak (5:15pm-6:15pm)


The PM peak period travel time results indicate the following:

- Overall, no notable change in performance of Canterbury Road (Route 7), with some travel time reductions for the eastbound direction and increases for the westbound direction. This is likely a result of the demand shifts experienced with the introduction of the bypass running with the current actuated traffic signal control configurations.
- As noted in the AM peak period, Evaline Street and Ninth Avenue (Route 5 and 6) experience increased overall travel times in both hours of the PM peak models.
- Significant benefits are observed, again particularly in the second hour of the peak period, for Beamish Street (Route 2 and 3). Travel time reductions are most significant in the second hour of the 2036 models, with overall travel time reductions of over $65 \%$ for Route 3 northbound through Beamish Street.


### 5.3.4. Network Congestion

The following section provides an overview of the overall network simulated density, highlighting critical locations causing network congestion.

Figure 5.18:Aimsun Future Base and Bypass Model Simulated Density - 2026 AM Peak (9:00am)


Figure 5.19:Aimsun Future Base and Bypass Model Simulated Density - 2036 AM Peak (9:00am)


Figure 5.20:Aimsun Future Base and Bypass Model Simulated Density - 2026 PM Peak (6:15pm)


Figure 5.21:Aimsun Future Base and Bypass Model Simulated Density - 2036 PM Peak (6:15pm)


The network congestion results show that the introduction of the bypass will have a two-fold impact:

- Reduction of observed congestion along Beamish Street through Campsie Town Centre.
- Increases in congestion for some of the east-west routes at the intersections with the bypass.


### 5.3.5. Changes in Traffic Volumes

Due to the introduction of the bypass, notable changes in traffic volumes for north-south routes are observed. To understand the key route diversions across the study area, volumes along the natural screenline created by the railway have been reviewed. These include the following locations (shown in Figure 5.22):

1. Loch Street (Bypass)
2. Beamish Street
3. Belombi Street.

Figure 5.22: North-South Screenline Locations for Volume Comparisons


Volume differences (2-hour) have been reviewed between the Bypass and Future Do Minimum scenarios across each design year and peak period. A summary of these volume differences is included in Table 5.4.

Table 5.4: Future Year - Changes in Traffic Volumes (2 hours)

| Scenario | Location 1 |  | Location 2 |  | Location 3 |  | Total |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NB | SB | NB | SB | NB | SB | NB | SB |
| 2026 AM | +889 | +830 | -573 | -221 | -76 | -83 | 240 | 526 |
| $2026 ~ P M ~$ | +840 | +833 | -554 | -10 | -6 | -13 | 280 | 810 |
| 2036 AM | +917 | +771 | -503 | -182 | -77 | -92 | 337 | 497 |
| 2036 PM | +980 | +781 | -450 | +56 | -26 | -129 | 504 | 708 |

The results show the following:

- The introduction of the bypass attracts additional north-south traffic volumes to Loch Street. The increase is in the order of 800-1,000 vehicles in two hours in the AM and PM peaks respectively.
- The bypass offers alternative north-south routes, mainly for through traffic which results in reduced traffic volumes along Beamish Street. The most pronounce reduction is recorded in the northbound direction in both peak periods.
- Overall, traffic volumes across the screenline increase in each future year which indicates that the proposed bypass will induce some addition trips from other corridors to travel through the study area.

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## 6. CONCLUSION



### 6.1. Conclusion

Based on the above discussions and findings regarding the Campsie Master Plan traffic modelling assessment, an overview of the key modelling outcomes are as follows:

- Future Do Minimum modelling:
- Traffic volumes within the study area will continue to grow at a rate of $2 \%$ p.a. until 2026. The rate of growth is expected to slow after 2026 to approximately $1 \%$ p.a.
- The forecast growth in traffic demands results will result in increased travel times and delays for the local road network around Campsie.
- With no changes to travel demands or road network infrastructure, travel times along Beamish Street northbound are likely to double in 2036
- Future Options Assessment:

This assessment has identified that implementing the Campsie Bypass would provide significant traffic improvements to Campsie by reducing traffic on Beamish Street by up to 500 vehicles over 2 hours and providing an alternative route for traffic moving north and south through the centre. Without the bypass, Beamish Street would be expected to be at capacity by 2036.

- The introduction of the bypass would require changes to a number of intersections with local road network to ensure that appropriate means of traffic control and priority are provided. The recommended changes to key intersections, as demonstrated within this report, will require further design investigations to determine if they are feasible within the available road environment or opportunities for land acquisition. If the intersection upgrades are not available, alternative measures to reduce the anticipated traffic volumes will be required by Council. Alternative measures could include improvements to walking, cycling and public transport accessibility and frequency. It is understood Council will commence a Complete Streets project, which will provide a more detailed analysis and recommendations for delivery of the Bypass and improvements to the local road network.
- As a result of additional traffic signals to support the bypass, some of the network statistics (average delays and travel times) would increase, however overall, the bypass will provide improvements to Beamish Street, in line with Council's aspirations to reduce regional throughtraffic along this road.
- The overall volumes within the study area would increase with the introduction of the bypass. These induced trips represent up to $2 \%$ of additional demands.
- The reduction in traffic volumes along Beamish Street is reflected in reduced congestion and significant travel time savings for northbound trips in 2026 and 2036 scenarios.

It is acknowledged that the draft Campsie Town Centre Master Plan comprises a number of measures to also support the reduction in congestion and traffic impacts to the local road network as a result of the forecast growth in Campsie. These include:

- The introduction of a maximum parking rate in the Campsie Town Centre core (sites within 400 metres of Campsie Station)
- A more flexible approach to parking outside of the core, with minimum and maximum parking rates
- The introduction of mandatory cycle parking
- Improved pedestrian and cycle network to make walking and cycling easier for the community to move around the town centre
- Advocacy to Transport for NSW for improved bus connectivity, particularly north-south between Campsie and Burwood

Collectively, these measures will encourage the community and users of the Campsie Town Centre to be less reliant on cars and maximise opportunities for active and passive transport use to achieve Council's long term modal-shift aspirations.

- Next steps
- This assessment has identified the proposed growth in Campsie under the revised draft masterplan and how this could be accommodated subject to improvements to the road network at the identified intersections.
- Further work will be undertaken as part of Council's Complete Streets project for Campsie to identify if the specific road network improvements needed to accommodate the predicted traffic growth along the proposed bypass and at other intersections are feasible and cost effective.
- Further work will also be undertaken as part of Council's Complete Streets project for Campsie to implement other measures to increase public transport usage such as reduced parking rates within close proximity to the metro station and to encourage walking and cycling.


## A. CALIBRATION AND VALIDATION REPORT


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## APPENDIX: CALIBRATION AND VALIDATION REPORT

## A.1. Convergence

The relative Gap (RGap) is a ratio of the actual travel time to the travel time when all vehicles use the shortest paths. The smaller the Rgap the better the convergence. For the purposes of this assessment, the RGap being $<0.5 \%$ was adopted. The model showed a satisfactory level of convergence as shown in Figure A. 1 and Figure A.2, with the AM and PM models reaching the required RGap criteria after 6 iterations.

Figure A.1: AM Model Convergence


Figure A.2: PM Model Convergence


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## A.2. Model Stability

In order to demonstrate the stability of the model, 5 seeds were run and used to determine a suitable median seed based on the VHT network statistics. The five seed values processed for both the AM and PM base model are listed in Table A. 1.

Table A.1: Model Seed Values (as per TfNSW Guidelines)

| Seed Number | Seed Value |
| :---: | :---: |
| 1 | 560 |
| 2 | 28 |
| 3 | 7771 |
| 4 | 86524 |
| 5 | 2849 |

The AM and PM peak model stability results are outlined in Table A. 3 and Table A.4.
Figure A.3: Median Seed Analysis - AM Peak


The results of the model stability analysis for the AM peak show acceptable variation in the VHT results, with the median seed recorded as seed value 86524.

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Figure A.4: Median Seed Analysis - PM Peak


The results of the model stability analysis for the PM peak show acceptable variation in the VHT results, with the median seed recorded as seed value 560.

## A.3. Calibration Results

A total of 31 link counts and 331 turn counts were utilised for both peak hours in the calibration process.
Table A. 2 shows the comparison of the observed and modelled link and turn traffic volumes for the AM and PM peak hours. The complete set of network wide traffic volume comparisons between observed and modelled data is provided as Appendix B.

Table A.2: Model Calibration Results


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The calibration results indicate that both the turn flow and link flow calibration appropriately meet criteria for both peak periods. There are a few turns that fall outside the GEH > 10 range, which are outlined below:

- AM Peak (8:30am-9:30am):
- There is 1 turn in the AM peak model with GEH > 10. This is for the southbound right turn from Duke Street on to Canterbury Road. This value has a GEH of 10.7; however, with the north approach signals running at least minimum green time, is deemed to not have a significant impact on the operation of the model.
- $\quad$ PM Peak (4:15pm-5:15pm):
- There is 1 turn in the PM peak model first hour with GEH > 10, which is observed for the Clissold Parade Eastbound right turn on to Beamish Street. The left turn at this approach calibrates appropriately and with the overall hourly count difference approximately 70 vehicles, this is not seen as a critical difference.
- $\quad$ PM Peak (5:15pm-6:15pm):
- 1 turn count in the second hour of the PM peak model has a GEH of 11 . This is seen at the Campsie Street westbound left turn at the roundabout with Loch Street. Again, the difference in count at this location has little bearing on the overall model performance.

It is also noted that in other seed runs, the GEH values at this location are less than 10, so are not considered critical to the model performance or overall model suitability.

In addition to the above, a modelled versus observed traffic volume (links) comparison has been undertaken in the form of a $R^{2}$ and scatter plot analysis for each of the peak hours. It is typically recommended that an $R^{2}$ value greater than 0.95 be achieved before a model is considered to be calibrated appropriately, whilst the guidelines recommend a value greater than 0.9.

Figure 6.5: Link Flow comparison All Vehicles - AM Peak (7:30am-8:30 am)


Figure 6.7: Link Flow comparison All Vehicles - PM Peak (4:15pm-5:15pm)


Figure 6.6: Link Flow comparison All Vehicles - AM Peak (8:30am-9:30am)


Figure 6.8: Link Flow comparison All Vehicles - PM Peak (5:15pm-6:15pm)


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Given the above, the results of the turn flow and link flow calibration meet the calibration criteria and are considered satisfactory for all peak periods.

## A.4. Travel Time Validation Results

Table A. 3 and Table A. 4 provide the travel time validation results for AM and PM peak hours, respectively. It is noted that the travel time criteria requires that Average modelled journey time to be within $15 \%$ or one minute (whichever is greater) of average observed journey time for full length of route.

Table A.3: Travel Time Validation Results - AM Peak

| Peak Period | Route | Direction | Average Observed Travel Time (s) | Average Modelled Travel Time (s) | Difference |  | Meets Criteria? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Relative (s) | \% |  |
| $\begin{aligned} & \text { 7:30am- } \\ & \text { 8:30am } \end{aligned}$ | Route 1 | Northbound | 456 | 416 | -40 | -9\% | Yes |
|  |  | Southbound | 419 | 403 | -16 | -4\% | Yes |
|  | Route 2 | Northbound | 544 | 518 | -26 | -5\% | Yes |
|  |  | Southbound | 527 | 523 | -5 | -1\% | Yes |
|  | Route 3 | Northbound | 465 | 399 | -66 | -14\% | Yes |
|  |  | Southbound | 398 | 362 | -37 | -9\% | Yes |
|  | Route 4 | Northbound | 231 | 240 | 9 | 4\% | Yes |
|  |  | Southbound | 341 | 306 | -34 | -10\% | Yes |
|  | Route 5 | Eastbound | 233 | 197 | -36 | -15\% | Yes |
|  |  | Westbound | 152 | 153 | 1 | 1\% | Yes |
|  | Route 6 | Eastbound | 232 | 200 | -32 | -14\% | Yes |
|  |  | Westbound | 231 | 193 | -38 | -17\% | Yes |
|  | Route 7 | Eastbound | 481 | 439 | -42 | -9\% | Yes |
|  |  | Westbound | 311 | 319 | 8 | 3\% | Yes |
| $\begin{aligned} & \text { 8:30am- } \\ & \text { 9:30am } \end{aligned}$ | Route 1 | Northbound | 452 | 413 | -40 | -9\% | Yes |
|  |  | Southbound | 441 | 410 | -31 | -7\% | Yes |
|  | Route 2 | Northbound | 574 | 535 | -39 | -7\% | Yes |
|  |  | Southbound | 596 | 608 | 11 | 2\% | Yes |
|  | Route 3 | Northbound | 468 | 414 | -54 | -11\% | Yes |
|  |  | Southbound | 424 | 453 | 29 | 7\% | Yes |
|  | Route 4 | Northbound | 214 | 242 | 27 | 13\% | Yes |
|  |  | Southbound | 275 | 293 | 18 | 7\% | Yes |
|  | Route 5 | Eastbound | 256 | 192 | -64 | -25\% | No |
|  |  | Westbound | 209 | 159 | -50 | -24\% | Yes |
|  | Route 6 | Eastbound | 321 | 199 | -122 | -38\% | No |
|  |  | Westbound | 262 | 198 | -64 | -25\% | No |
|  | Route 7 | Eastbound | 389 | 341 | -48 | -12\% | Yes |
|  |  | Westbound | 311 | 322 | 11 | 4\% | Yes |

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Table A.4: Travel Time Validation Results - PM Peak

| Peak Period | Route | Direction | Average Observed Travel Time (s) | Average Modelled Travel Time (s) | Difference |  | Meets Criteria? |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Relative (s) | \% |  |
| $\begin{aligned} & 4: 15 \mathrm{pm}- \\ & 5: 15 \mathrm{pm} \end{aligned}$ | Route 1 | Northbound | 454 | 419 | -35 | -8\% | Yes |
|  |  | Southbound | 489 | 428 | -61 | -13\% | Yes |
|  | Route 2 | Northbound | 606 | 584 | -22 | -4\% | Yes |
|  |  | Southbound | 675 | 574 | -100 | -15\% | Yes |
|  | Route 3 | Northbound | 462 | 448 | -14 | -3\% | Yes |
|  |  | Southbound | 511 | 418 | -93 | -18\% | No |
|  | Route 4 | Northbound | 220 | 239 | 19 | 9\% | Yes |
|  |  | Southbound | 312 | 291 | -20 | -6\% | Yes |
|  | Route 5 | Eastbound | 266 | 195 | -71 | -27\% | No |
|  |  | Westbound | 233 | 180 | -54 | -23\% | Yes |
|  | Route 6 | Eastbound | 300 | 198 | -101 | -34\% | No |
|  |  | Westbound | 274 | 198 | -76 | -28\% | No |
|  | Route 7 | Eastbound | 307 | 282 | -25 | -8\% | Yes |
|  |  | Westbound | 341 | 344 | 3 | 1\% | Yes |
| $\begin{aligned} & 5: 15 \mathrm{pm}- \\ & 6: 15 \mathrm{pm} \end{aligned}$ | Route 1 | Northbound | 446 | 414 | -32 | -7\% | Yes |
|  |  | Southbound | 453 | 420 | -32 | -7\% | Yes |
|  | Route 2 | Northbound | 650 | 702 | 52 | 8\% | Yes |
|  |  | Southbound | 693 | 524 | -169 | -24\% | No |
|  | Route 3 | Northbound | 511 | 507 | -4 | -1\% | Yes |
|  |  | Southbound | 491 | 370 | -121 | -25\% | No |
|  | Route 4 | Northbound | 226 | 243 | 17 | 8\% | Yes |
|  |  | Southbound | 291 | 286 | -5 | -2\% | Yes |
|  | Route 5 | Eastbound | 243 | 194 | -49 | -20\% | Yes |
|  |  | Westbound | 235 | 241 | 6 | 3\% | Yes |
|  | Route 6 | Eastbound | 408 | 207 | -200 | -49\% | No |
|  |  | Westbound | 261 | 213 | -47 | -18\% | Yes |
|  | Route 7 | Eastbound | 289 | 300 | 10 | 4\% | Yes |
|  |  | Westbound | 337 | 313 | -24 | -7\% | Yes |

The travel time results are also graphically presented in Appendix C.
In general, the modelled travel time are within acceptable range except for the routes detailed below.
Route 2 - Lees Avenue, Second Avenue, Ninth Avenue, Beamish Street and Bexley Road
Route 2 (Southbound) modelled timings are faster than observed average travel times in the second PM peak hour ( $5: 15 \mathrm{pm}$ to $6: 15 \mathrm{pm}$ ) between Linthorn Avenue and Cross Street as presented in Figure A.9.

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Figure A.9: Route 2, Southbound ( $5: 15 \mathrm{pm}-6: 15 \mathrm{pm}$ )


## Route 3 - Brighton Avenue, Beamish Street and Bexley Road

Route 3 (Southbound) modelled timings are faster than observed average travel times in both PM peak hours between Albert Street and Cross Street as presented in Figure A. 10 and Figure A.11.

Figure A.10: Route 3, Southbound (4:15pm-5:15pm)


Figure A.11: Route 3, Southbound (5:15pm-6:15pm)


It is seen in the Figures above that the PM peak model travel times for routes 2 and 3 show less delay through the cente of Campsie; hwoever are within the minimum range of the obesrved travel times and only marginally outside the $15 \%$ margins.

## Route 5 - Albert Street and Ninth Avenue

Route 5 (Eastbound) modelled timings are faster than observed average travel times in the second AM peak hour (8:30am to 9:30am) and first PM peak (4:15pm to 5:15pm) between Cecelia Street and Beamish Street. These are presented in Figure A. 12 and Figure A. 13.

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Figure A.12: Route 5, Eastbound (8:30am-9:30am)


Figure A.13: Route 5, Eastbound (4:15pm-5:15pm)


As noted with routes 2 and 3 , the modelled travel times for route 5 eastbound fall just outside the required criteria; however, are still within the minimum observed travel times.

Route 6 - Evaline Street
Route 6 modelled timings between Loftus Street and Wonga Street are consistently faster than observed average travel times for both directions during the second AM peak hour (8:30am to 9:30am) as presented in Figure A. 14 and Figure A. 15.

Figure A.14: Route 6, Eastbound (8:30am-9:30am)


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Figure A.15: $\quad$ Route 6, Westbound (8:30am-9:30am)


Furthermore, modelled timings for both eastbound and westbound directions during the first PM peak ( $4: 15 \mathrm{pm}-5: 15 \mathrm{pm}$ ) and eastbound during the second PM peak ( $5: 15 \mathrm{pm}-6: 15 \mathrm{pm}$ ) are faster than average observed travel times, presented in Figure A.16, Figure A.17, and Figure A. 18.

Figure A.16: Route 6, Eastbound (4:15pm-5:15pm)


Figure A.17: Route 6, Westbound (4:15pm-5:15pm)


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Figure A.18: Route 6, Eastbound (5:15pm-6:15pm)


It is noted there is a consistent mismatch for the Evaline Street (route 6) travel times, particularly with the interactions at Beamish Street and the signalised pedestrian crossing at the shopping centre. It is noted, that in some instances there is a lack of observed vehicle runs contributing to these averages, with higher observed times then significantly affecting the average. This is seen for the second hour of the PM peak in the eastbound direction, where only 3 runs were observed, one with greater than a 7 minute travel time for the second segment along Evaline Street, suggesting this vehicle missed more than 3 cycle times at these traffic lights.

## A.5. Congestion Hot Spots

A comparison between Google Traffic maps and simulated model density plots is presented in Figure A. 19 and Figure A. 20 for the AM and PM peak hour, respectively.

Figure A.19: AM Peak Congestion Comparison - 8:30am


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Figure A.20: PM Peak Congestion Comparison - 5:00pm


As presented above, in general the model congestion locations are similar in nature to that estimated by Google Traffic. The congestion hot spots are similar, with most of the locations observed along Canterbury Road and the arterial roads through Campsie.

## A.6. Model Limitations

In general, the model provides a good representation of existing conditions, however it is recognised that meso models may not adequately represent:

- delays relating to interactions between pedestrians and cars
- delays relating to drivers slowing down to look for parking spaces or giving way to vehicles parallel parking
- weaving and merging delays.

Meso models may generally be faster around sections with the interactions outlined above. Therefore, the model travel times can be expected to be faster or predict less delays at some locations which is recognised and outlined in the context of this report.

For a study area of this size and the strategic nature of the study, a mesoscopic model was considered to be an appropriate tool and represents and adequate level of delays and congestion for the study purpose.

## A.7. Conclusion

This section of the report has presented the calibration and validation results of the Aimsun mesoscopic model for Campsie. The results presented show that the model demonstrates reasonable 'goodness of fit' with the observed traffic conditions, which indicates that the model performs well at the network wide level.

The traffic volume comparisons for each of the peaks indicate a high level of correlation between the modelled and observed traffic flows with almost all of the targets being met.

The travel time analysis illustrates a reasonably good level of correlation between the modelled and observed travel times, with any discrepancies considered to have minimal impact on the overall project.

It is our view that the model is successfully calibrated and validated and is fit for its intended purpose.

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## B.CALIBRATION RESULTS

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| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 106372 | 238 | 138 | 213 | 138 | -25 | 0 | 1.7 | 0.0 |
| 106373 | 166 | 156 | 181 | 169 | 15 | 13 | 1.1 | 1.0 |
| 106374 | 54 | 51 | 45 | 41 | -9 | -10 | 1.3 | 1.5 |
| 106375 | 35 | 37 | 41 | 37 | 6 | 0 | 1.0 | 0.0 |
| 106376 | 210 | 255 | 213 | 268 | 3 | 13 | 0.2 | 0.8 |
| 106377 | 130 | 136 | 127 | 132 | -3 | -4 | 0.3 | 0.3 |
| 106378 | 27 | 34 | 2 | 5 | -25 | -29 | 6.6 | 6.6 |
| 106379 | 12 | 31 | 4 | 4 | -8 | -27 | 2.8 | 6.5 |
| 106380 | 18 | 27 | 14 | 21 | -4 | -6 | 1.0 | 1.2 |
| 106381 | 101 | 81 | 101 | 89 | 0 | 8 | 0.0 | 0.9 |
| 106382 | 6 | 8 | 7 | 9 | 1 | 1 | 0.4 | 0.3 |
| 106383 | 45 | 53 | 5 | 6 | -40 | -47 | 8.0 | 8.7 |
| 106384 | 60 | 41 | 76 | 77 | 16 | 36 | 1.9 | 4.7 |
| 106386 | 15 | 18 | 22 | 38 | 7 | 20 | 1.6 | 3.8 |
| 106385 | 43 | 33 | 51 | 39 | 8 | 6 | 1.2 | 1.0 |
| 106387 | 87 | 102 | 146 | 153 | 59 | 51 | 5.5 | 4.5 |
| 106388 | 49 | 53 | 18 | 33 | -31 | -20 | 5.4 | 3.0 |
| 106389 | 69 | 121 | 66 | 127 | -3 | 6 | 0.4 | 0.5 |
| 106390 | 29 | 63 | 26 | 72 | -3 | 9 | 0.6 | 1.1 |
| 106391 | 41 | 55 | 42 | 58 | 1 | 3 | 0.2 | 0.4 |
| 106392 | 45 | 47 | 57 | 45 | 12 | -2 | 1.7 | 0.3 |
| 106393 | 322 | 309 | 415 | 396 | 93 | 87 | 4.8 | 4.6 |
| 106394 | 222 | 193 | 164 | 184 | -58 | -9 | 4.2 | 0.7 |
| 106395 | 955 | 791 | 963 | 830 | 8 | 39 | 0.3 | 1.4 |
| 106396 | 402 | 404 | 414 | 403 | 12 | -1 | 0.6 | 0.0 |
| 106397 | 1,306 | 1,126 | 1,309 | 1,166 | 3 | 40 | 0.1 | 1.2 |
| 106398 | 817 | 743 | 844 | 760 | 27 | 17 | 0.9 | 0.6 |
| 106399 | 1,755 | 1,670 | 1,731 | 1,783 | -24 | 113 | 0.6 | 2.7 |
| 106400 | 1,156 | 1,153 | 1,155 | 1,148 | -1 | -5 | 0.0 | 0.1 |
| 106401 | 968 | 901 | 991 | 922 | 23 | 21 | 0.7 | 0.7 |
| 106402 | 670 | 639 | 695 | 647 | 25 | 8 | 1.0 | 0.3 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 106372 | 1 | 3 | 7 | 5 | 6 | 2 | 3.0 | 1.0 |
| 106373 | 14 | 13 | 11 | 14 | -3 | 1 | 0.8 | 0.3 |
| 106374 | 3 | 3 | 3 | 5 | 0 | 2 | 0.0 | 1.0 |
| 106375 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 106376 | 10 | 6 | 7 | 4 | -3 | -2 | 1.0 | 0.9 |
| 106377 | 3 | 3 | 2 | 5 | -1 | 2 | 0.6 | 1.0 |
| 106378 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 106379 | 1 | 3 | - | - | -1 | -3 | 1.4 | 2.4 |
| 106380 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106381 | 4 | 4 | 5 | 2 | 1 | -2 | 0.5 | 1.2 |
| 106382 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106383 | 4 | 7 | - | - | -4 | -7 | 2.8 | 3.7 |
| 106384 | 1 | - | 6 | 4 | 5 | 4 | 2.7 | 2.8 |
| 106386 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106385 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 106387 | 3 | 6 | 3 | 3 | 0 | -3 | 0.0 | 1.4 |
| 106388 | 5 | 15 | - | - | -5 | -15 | 3.2 | 5.5 |
| 106389 | 6 | 4 | - | - | -6 | -4 | 3.5 | 2.8 |
| 106390 | 3 | 8 | - | - | -3 | -8 | 2.4 | 4.0 |
| 106391 | 3 | 3 | 2 | 4 | -1 | 1 | 0.6 | 0.5 |
| 106392 | 5 | 5 | - | - | -5 | -5 | 3.2 | 3.2 |
| 106393 | 9 | 47 | 2 | 17 | -7 | -30 | 3.0 | 5.3 |
| 106394 | 18 | 23 | 2 | 6 | -16 | -17 | 5.1 | 4.5 |
| 106395 | 27 | 39 | 26 | 39 | -1 | 0 | 0.2 | 0.0 |
| 106396 | 18 | 24 | 18 | 22 | 0 | -2 | 0.0 | 0.4 |
| 106397 | 128 | 77 | 98 | 75 | -30 | -2 | 2.8 | 0.2 |
| 106398 | 83 | 86 | 73 | 68 | -10 | -18 | 1.1 | 2.1 |
| 106399 | 88 | 82 | 90 | 87 | 2 | 5 | 0.2 | 0.5 |
| 106400 | 67 | 71 | 65 | 72 | -2 | 1 | 0.2 | 0.1 |
| 106401 | 44 | 43 | 49 | 46 | 5 | 3 | 0.7 | 0.4 |
| 106402 | 49 | 47 | 56 | 45 | 7 | -2 | 1.0 | 0.3 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 8657 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 8658 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 8656 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 8652 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8650 | 206 | 306 | 214 | 310 | 8 | 4 | 0.6 | 0.2 |
| 8651 | 22 | 29 | 45 | 44 | 23 | 15 | 4.0 | 2.5 |
| 8653 | 37 | 42 | - | 29 | -37 | -13 | 8.6 | 2.2 |
| 8655 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 8654 | 37 | 44 | 13 | 33 | -24 | -11 | 4.8 | 1.8 |
| 8648 | 24 | 34 | 30 | 29 | 6 | -5 | 1.2 | 0.9 |
| 8646 | 400 | 368 | 395 | 382 | -5 | 14 | 0.3 | 0.7 |
| 8649 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 8750 | 13 | 12 | 24 | 21 | 11 | 9 | 2.6 | 2.2 |
| 8752 | 1 | 10 | 8 | 9 | 7 | -1 | 3.3 | 0.3 |
| 8753 | 207 | 298 | 237 | 330 | 30 | 32 | 2.0 | 1.8 |
| 8802 | 61 | 70 | 54 | 63 | -7 | -7 | 0.9 | 0.9 |
| 6970 | 74 | 97 | 62 | 79 | -12 | -18 | 1.5 | 1.9 |
| 8780 | 16 | 22 | 1 | 1 | -15 | -21 | 5.1 | 6.2 |
| 8782 | 389 | 359 | 393 | 406 | 4 | 47 | 0.2 | 2.4 |
| 7119 | 13 | 10 | 4 | 10 | -9 | 0 | 3.1 | 0.0 |
| 7118 | 411 | 287 | 420 | 320 | 9 | 33 | 0.4 | 1.9 |
| 7117 | 9 | 14 | 3 | 8 | -6 | -6 | 2.4 | 1.8 |
| 7112 | - | 8 | 1 | 2 | 1 | -6 | 1.4 | 2.7 |
| 7113 | 78 | 107 | 56 | 98 | -22 | -9 | 2.7 | 0.9 |
| 7110 | 83 | 96 | 79 | 82 | -4 | -14 | 0.4 | 1.5 |
| 7114 | 80 | 110 | 78 | 113 | -2 | 3 | 0.2 | 0.3 |
| 7115 | 261 | 258 | 271 | 281 | 10 | 23 | 0.6 | 1.4 |
| 7116 | 50 | 56 | 51 | 44 | 1 | -12 | 0.1 | 1.7 |
| 7121 | 67 | 66 | 75 | 81 | 8 | 15 | 0.9 | 1.7 |
| 7120 | 183 | 171 | 160 | 162 | -23 | -9 | 1.8 | 0.7 |
| 7122 | 6 | 12 | 27 | 20 | 21 | 8 | 5.2 | 2.0 |
| 7162 | 3 | 8 | 4 | 23 | 1 | 15 | 0.5 | 3.8 |
| 7164 | 415 | 295 | 422 | 320 | 7 | 25 | 0.3 | 1.4 |
| 7165 | 14 | 17 | 7 | 11 | -7 | -6 | 2.2 | 1.6 |
| 7149 | 22 | 22 | 26 | 22 | 4 | 0 | 0.8 | 0.0 |
| 7148 | 250 | 265 | 279 | 281 | 29 | 16 | 1.8 | 1.0 |
| 7145 | 15 | 20 | 14 | 13 | -1 | -7 | 0.3 | 1.7 |
| 105919 | 21 | 44 | 20 | 38 | -1 | -6 | 0.2 | 0.9 |
| 105920 | 137 | 192 | 133 | 193 | -4 | 1 | 0.3 | 0.1 |
| 105923 | 289 | 271 | 313 | 305 | 24 | 34 | 1.4 | 2.0 |
| 105924 | 1 | 6 | - | - | -1 | -6 | 1.4 | 3.5 |
| 105922 | - | 6 | - | - | 0 | -6 | 0.0 | 3.5 |
| 105921 | 47 | 37 | 37 | 37 | -10 | 0 | 1.5 | 0.0 |
| 6235 | 166 | 203 | 193 | 260 | 27 | 57 | 2.0 | 3.7 |
| 6234 | 273 | 185 | 275 | 234 | 2 | 49 | 0.1 | 3.4 |
| 6233 | 165 | 155 | 177 | 157 | 12 | 2 | 0.9 | 0.2 |
| 6231 | 102 | 133 | 101 | 141 | -1 | 8 | 0.1 | 0.7 |
| 13115 | 139 | 117 | 152 | 108 | 13 | -9 | 1.1 | 0.8 |
| 6237 | 342 | 297 | 428 | 384 | 86 | 87 | 4.4 | 4.7 |
| 11531 | 373 | 281 | 332 | 297 | -41 | 16 | 2.2 | 0.9 |
| 11529 | 345 | 292 | 265 | 209 | -80 | -83 | 4.6 | 5.2 |
| 11532 | 269 | 325 | 325 | 356 | 56 | 31 | 3.2 | 1.7 |
| 11533 | 64 | 118 | 112 | 178 | 48 | 60 | 5.1 | 4.9 |
| 11535 | 210 | 138 | 226 | 148 | 16 | 10 | 1.1 | 0.8 |
| 11534 | 296 | 300 | 370 | 387 | 74 | 87 | 4.1 | 4.7 |
| 9844 | 615 | 489 | 523 | 445 | -92 | -44 | 3.9 | 2.0 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 13205 | 53 | 78 | 57 | 71 | 4 | -7 | 0.5 | 0.8 |
| 13203 | 31 | 45 | 5 | 16 | -26 | -29 | 6.1 | 5.3 |
| 13204 | 41 | 58 | 21 | 28 | -20 | -30 | 3.6 | 4.6 |
| 13202 | 29 | 42 | 11 | 4 | -18 | -38 | 4.0 | 7.9 |
| 9846 | 523 | 559 | 647 | 673 | 124 | 114 | 5.1 | 4.6 |
| 105935 | 50 | 46 | 48 | 44 | -2 | -2 | 0.3 | 0.3 |
| 105937 | 632 | 542 | 538 | 502 | -94 | -40 | 3.9 | 1.8 |
| 105931 | 41 | 48 | 62 | 51 | 21 | 3 | 2.9 | 0.4 |
| 105933 | 24 | 26 | 14 | 23 | -10 | -3 | 2.3 | 0.6 |
| 105934 | 539 | 578 | 638 | 667 | 99 | 89 | 4.1 | 3.6 |
| 105927 | 39 | 18 | 44 | 15 | 5 | -3 | 0.8 | 0.7 |
| 13265 | 538 | 467 | 510 | 481 | -28 | 14 | 1.2 | 0.6 |
| 13266 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 13268 | 31 | 50 | 11 | 25 | -20 | -25 | 4.4 | 4.1 |
| 13267 | 110 | 111 | 37 | 52 | -73 | -59 | 8.5 | 6.5 |
| 13262 | 173 | 183 | 176 | 207 | 3 | 24 | 0.2 | 1.7 |
| 13261 | 391 | 450 | 525 | 512 | 134 | 62 | 6.3 | 2.8 |
| 13263 | 41 | 14 | 38 | 15 | -3 | 1 | 0.5 | 0.3 |
| 13264 | 42 | 45 | 2 | - | -40 | -45 | 8.5 | 9.5 |
| 10017 | 13 | 5 | 10 | 4 | -3 | -1 | 0.9 | 0.5 |
| 7261 | 52 | 96 | 23 | 48 | -29 | -48 | 4.7 | 5.7 |
| 7262 | 512 | 403 | 491 | 426 | -21 | 23 | 0.9 | 1.1 |
| 7260 | 432 | 500 | 550 | 538 | 118 | 38 | 5.3 | 1.7 |
| 7256 | 17 | 50 | 19 | 52 | 2 | 2 | 0.5 | 0.3 |
| 5943 | 62 | 57 | 100 | 75 | 38 | 18 | 4.2 | 2.2 |
| 5944 | 476 | 380 | 447 | 387 | -29 | 7 | 1.3 | 0.4 |
| 13473 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 5950 | 18 | 27 | 22 | 15 | 4 | -12 | 0.9 | 2.6 |
| 5949 | 87 | 128 | 61 | 143 | -26 | 15 | 3.0 | 1.3 |
| 5951 | 49 | 69 | 25 | 34 | -24 | -35 | 3.9 | 4.9 |
| 5948 | 32 | 51 | 42 | 28 | 10 | -23 | 1.6 | 3.7 |
| 5947 | 355 | 388 | 477 | 458 | 122 | 70 | 6.0 | 3.4 |
| 5946 | 39 | 62 | 29 | 47 | -10 | -15 | 1.7 | 2.0 |
| 5941 | 32 | 53 | 34 | 51 | 2 | -2 | 0.3 | 0.3 |
| 5942 | 112 | 131 | 104 | 111 | -8 | -20 | 0.8 | 1.8 |
| 5939 | 82 | 107 | 58 | 78 | -24 | -29 | 2.9 | 3.0 |
| 105946 | 24 | 37 | 18 | 28 | -6 | -9 | 1.3 | 1.6 |
| 105947 | 514 | 392 | 487 | 367 | -27 | -25 | 1.2 | 1.3 |
| 105945 | 17 | 44 | 16 | 43 | -1 | -1 | 0.2 | 0.2 |
| 105941 | 18 | 29 | 16 | 34 | -2 | 5 | 0.5 | 0.9 |
| 105939 | - | - | 2 | 2 | 2 | 2 | 2.0 | 2.0 |
| 105940 | - | - | 22 | 21 | 22 | 21 | 6.6 | 6.5 |
| 105948 | 14 | 31 | 14 | 4 | 0 | -27 | 0.0 | 6.5 |
| 105950 | 415 | 442 | 515 | 474 | 100 | 32 | 4.6 | 1.5 |
| 105949 | 25 | 49 | 30 | 73 | 5 | 24 | 1.0 | 3.1 |
| 105943 | 37 | 50 | 43 | 73 | 6 | 23 | 0.9 | 2.9 |
| 105942 | 43 | 43 | 6 | 40 | -37 | -3 | 7.5 | 0.5 |
| 105944 | 22 | 34 | 15 | 6 | -7 | -28 | 1.6 | 6.3 |
| 7358 | 44 | 30 | 42 | 27 | -2 | -3 | 0.3 | 0.6 |
| 7359 | 596 | 556 | 627 | 568 | 31 | 12 | 1.3 | 0.5 |
| 7361 | 376 | 375 | 345 | 342 | -31 | -33 | 1.6 | 1.7 |
| 7360 | 23 | 9 | 16 | 16 | -7 | 7 | 1.6 | 2.0 |
| 7355 | 56 | 28 | 53 | 24 | -3 | -4 | 0.4 | 0.8 |
| 7357 | 16 | 18 | 15 | 9 | -1 | -9 | 0.3 | 2.4 |
| 8485 | 21 | 18 | 18 | 11 | -3 | -7 | 0.7 | 1.8 |
| 8483 | 349 | 308 | 385 | 352 | 36 | 44 | 1.9 | 2.4 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 8484 | 63 | 40 | 20 | 15 | -43 | -25 | 6.7 | 4.8 |
| 8487 | 33 | 49 | 46 | 43 | 13 | -6 | 2.1 | 0.9 |
| 8488 | 772 | 784 | 803 | 804 | 31 | 20 | 1.1 | 0.7 |
| 8486 | 228 | 162 | 205 | 135 | -23 | -27 | 1.6 | 2.2 |
| 8481 | 80 | 70 | 70 | 39 | -10 | -31 | 1.2 | 4.2 |
| 8479 | 239 | 234 | 252 | 246 | 13 | 12 | 0.8 | 0.8 |
| 8482 | 48 | 61 | 26 | 41 | -22 | -20 | 3.6 | 2.8 |
| 8489 | 137 | 144 | 136 | 129 | -1 | -15 | 0.1 | 1.3 |
| 8491 | 1,179 | 1,050 | 1,182 | 1,035 | 3 | -15 | 0.1 | 0.5 |
| 8375 | 1,068 | 1,057 | 1,030 | 985 | -38 | -72 | 1.2 | 2.3 |
| 8374 | 4 | 5 | - | - | -4 | -5 | 2.8 | 3.2 |
| 8369 | 41 | 55 | 27 | 60 | -14 | 5 | 2.4 | 0.7 |
| 8371 | 4 | 4 | 11 | 34 | 7 | 30 | 2.6 | 6.9 |
| 8372 | 21 | 17 | 7 | 22 | -14 | 5 | 3.7 | 1.1 |
| 8373 | 1,317 | 1,103 | 1,258 | 1,068 | -59 | -35 | 1.6 | 1.1 |
| 8466 | 85 | 88 | 100 | 90 | 15 | 2 | 1.6 | 0.2 |
| 8465 | 571 | 512 | 579 | 510 | 8 | -2 | 0.3 | 0.1 |
| 8463 | 312 | 301 | 312 | 321 | 0 | 20 | 0.0 | 1.1 |
| 8467 | 140 | 125 | 108 | 136 | -32 | 11 | 2.9 | 1.0 |
| 8469 | 804 | 816 | 780 | 791 | -24 | -25 | 0.9 | 0.9 |
| 5954 | 29 | 51 | 78 | 82 | 49 | 31 | 6.7 | 3.8 |
| 8470 | 323 | 300 | 379 | 315 | 56 | 15 | 3.0 | 0.9 |
| 8472 | 82 | 92 | 133 | 89 | 51 | -3 | 4.9 | 0.3 |
| 8475 | 48 | 72 | 24 | 46 | -24 | -26 | 4.0 | 3.4 |
| 8474 | 1,069 | 899 | 1,034 | 877 | -35 | -22 | 1.1 | 0.7 |
| 8473 | 207 | 214 | 213 | 198 | 6 | -16 | 0.4 | 1.1 |
| 8355 | 16 | 5 | - | - | -16 | -5 | 5.7 | 3.2 |
| 8353 | - | - | 3 | 1 | 3 | 1 | 2.4 | 1.4 |
| 8354 | 1 | 2 | 6 | 5 | 5 | 3 | 2.7 | 1.6 |
| 8357 | 37 | 26 | 34 | 76 | -3 | 50 | 0.5 | 7.0 |
| 8358 | 929 | 939 | 861 | 927 | -68 | -12 | 2.3 | 0.4 |
| 8351 | 14 | 13 | 24 | 15 | 10 | 2 | 2.3 | 0.5 |
| 8349 | - | - | 9 | - | 9 | 0 | 4.2 | 0.0 |
| 8352 | - | - | 21 | 9 | 21 | 9 | 6.5 | 4.2 |
| 8359 | 16 | 24 | 19 | 19 | 3 | -5 | 0.7 | 1.1 |
| 8361 | 1,384 | 1,237 | 1,396 | 1,270 | 12 | 33 | 0.3 | 0.9 |
| 8394 | 1,136 | 1,066 | 1,090 | 1,000 | -46 | -66 | 1.4 | 2.1 |
| 8390 | - | - | 5 | 5 | 5 | 5 | 3.2 | 3.2 |
| 8392 | 106 | 87 | 58 | 12 | -48 | -75 | 5.3 | 10.7 |
| 8395 | 17 | 30 | 19 | 48 | 2 | 18 | 0.5 | 2.9 |
| 8396 | 1,390 | 1,312 | 1,400 | 1,348 | 10 | 36 | 0.3 | 1.0 |
| 11250 | 1,107 | 1,035 | 1,083 | 1,027 | -24 | -8 | 0.7 | 0.2 |
| 11249 | 194 | 213 | 178 | 223 | -16 | 10 | 1.2 | 0.7 |
| 11246 | 230 | 220 | 201 | 248 | -29 | 28 | 2.0 | 1.8 |
| 11248 | 88 | 90 | 45 | 68 | -43 | -22 | 5.3 | 2.5 |
| 11251 | 18 | 35 | 18 | 31 | 0 | -4 | 0.0 | 0.7 |
| 11252 | 1,537 | 1,366 | 1,519 | 1,422 | -18 | 56 | 0.5 | 1.5 |
| 7813 | 91 | 189 | 112 | 201 | 21 | 12 | 2.1 | 0.9 |
| 7811 | 152 | 244 | 155 | 250 | 3 | 6 | 0.2 | 0.4 |
| 7814 | 76 | 114 | 69 | 115 | -7 | 1 | 0.8 | 0.1 |
| 7815 | 1,080 | 1,039 | 1,100 | 1,040 | 20 | 1 | 0.6 | 0.0 |
| 7817 | 1,603 | 1,426 | 1,584 | 1,509 | -19 | 83 | 0.5 | 2.2 |
| 7816 | 136 | 172 | 151 | 176 | 15 | 4 | 1.3 | 0.3 |
| 105321 | 9 | 15 | 9 | 21 | 0 | 6 | 0.0 | 1.4 |
| 105322 | 78 | 67 | 74 | 64 | -4 | -3 | 0.5 | 0.4 |
| 105323 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 105320 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105317 | 17 | 13 | 14 | 13 | -3 | 0 | 0.8 | 0.0 |
| 105318 | 47 | 29 | 49 | 29 | 2 | 0 | 0.3 | 0.0 |
| 105315 | 31 | 62 | 33 | 63 | 2 | 1 | 0.4 | 0.1 |
| 105316 | 61 | 76 | 72 | 84 | 11 | 8 | 1.3 | 0.9 |
| 105313 | 33 | 51 | 32 | 45 | -1 | -6 | 0.2 | 0.9 |
| 105310 | 67 | 68 | 67 | 68 | 0 | 0 | 0.0 | 0.0 |
| 105311 | 26 | 21 | 25 | 20 | -1 | -1 | 0.2 | 0.2 |
| 105312 | 6 | 5 | 23 | 17 | 17 | 12 | 4.5 | 3.6 |
| 105309 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105324 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105319 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105314 | 1 | 4 | - | - | -1 | -4 | 1.4 | 2.8 |
| 105441 | 13 | 23 | 13 | 12 | 0 | -11 | 0.0 | 2.6 |
| 105438 | 378 | 295 | 384 | 311 | 6 | 16 | 0.3 | 0.9 |
| 105439 | 19 | 26 | 8 | - | -11 | -26 | 3.0 | 7.2 |
| 105436 | 29 | 34 | 13 | 16 | -16 | -18 | 3.5 | 3.6 |
| 105437 | 85 | 117 | 74 | 110 | -11 | -7 | 1.2 | 0.7 |
| 105434 | 45 | 29 | 41 | 47 | -4 | 18 | 0.6 | 2.9 |
| 105431 | 38 | 36 | 51 | 57 | 13 | 21 | 1.9 | 3.1 |
| 105432 | 271 | 297 | 281 | 292 | 10 | -5 | 0.6 | 0.3 |
| 105433 | 22 | 22 | 27 | 20 | 5 | -2 | 1.0 | 0.4 |
| 105442 | 73 | 92 | 70 | 99 | -3 | 7 | 0.4 | 0.7 |
| 105443 | 189 | 173 | 187 | 182 | -2 | 9 | 0.1 | 0.7 |
| 105444 | 21 | 24 | 1 | 2 | -20 | -22 | 6.0 | 6.1 |
| 105445 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105440 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105435 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105430 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105877 | 77 | 117 | 70 | 108 | -7 | -9 | 0.8 | 0.8 |
| 105876 | 475 | 308 | 420 | 248 | -55 | -60 | 2.6 | 3.6 |
| 105878 | 215 | 299 | 300 | 372 | 85 | 73 | 5.3 | 4.0 |
| 105880 | 85 | 127 | 83 | 123 | -2 | -4 | 0.2 | 0.4 |
| 105882 | 212 | 183 | 210 | 180 | -2 | -3 | 0.1 | 0.2 |
| 105881 | 125 | 129 | 138 | 164 | 13 | 35 | 1.1 | 2.9 |
| 105875 | 2 | 6 | - | - | -2 | -6 | 2.0 | 3.5 |
| 105879 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 105883 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105520 | 22 | 24 | 36 | 27 | 14 | 3 | 2.6 | 0.6 |
| 105522 | 316 | 253 | 386 | 338 | 70 | 85 | 3.7 | 4.9 |
| 105524 | 136 | 164 | 134 | 165 | -2 | 1 | 0.2 | 0.1 |
| 105523 | 250 | 371 | 271 | 372 | 21 | 1 | 1.3 | 0.1 |
| 105519 | 616 | 437 | 558 | 386 | -58 | -51 | 2.4 | 2.5 |
| 105518 | 25 | 16 | 15 | 17 | -10 | 1 | 2.2 | 0.2 |
| 105517 | 4 | 2 | - | - | -4 | -2 | 2.8 | 2.0 |
| 105521 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105525 | 4 | 6 | - | - | -4 | -6 | 2.8 | 3.5 |
| 105579 | 212 | 211 | 213 | 199 | 1 | -12 | 0.1 | 0.8 |
| 105577 | 537 | 432 | 564 | 453 | 27 | 21 | 1.2 | 1.0 |
| 105575 | 393 | 445 | 416 | 473 | 23 | 28 | 1.1 | 1.3 |
| 105576 | 130 | 192 | 120 | 200 | -10 | 8 | 0.9 | 0.6 |
| 105580 | 241 | 202 | 294 | 256 | 53 | 54 | 3.2 | 3.6 |
| 105581 | 240 | 312 | 177 | 256 | -63 | -56 | 4.4 | 3.3 |
| 105582 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105578 | 2 | 4 | - | - | -2 | -4 | 2.0 | 2.8 |
| 105574 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 105602 | 220 | 292 | 240 | 342 | 20 | 50 | 1.3 | 2.8 |
| 106312 | 38 | 33 | 65 | 58 | 27 | 25 | 3.8 | 3.7 |
| 105598 | 41 | 45 | 50 | 51 | 9 | 6 | 1.3 | 0.9 |
| 105599 | 307 | 336 | 296 | 333 | -11 | -3 | 0.6 | 0.2 |
| 106313 | 361 | 305 | 365 | 306 | 4 | 1 | 0.2 | 0.1 |
| 105604 | 414 | 338 | 493 | 405 | 79 | 67 | 3.7 | 3.5 |
| 105605 | - | 3 | - | - | 0 | -3 | 0.0 | 2.4 |
| 105601 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 106311 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105550 | 24 | 38 | 17 | 37 | -7 | -1 | 1.5 | 0.2 |
| 105551 | 310 | 259 | 403 | 356 | 93 | 97 | 4.9 | 5.5 |
| 105548 | 13 | 12 | 5 | 5 | -8 | -7 | 2.7 | 2.4 |
| 105545 | 25 | 19 | 4 | 12 | -21 | -7 | 5.5 | 1.8 |
| 105546 | 7 | 8 | 1 | 6 | -6 | -2 | 3.0 | 0.8 |
| 105547 | 1 | - | 21 | 10 | 20 | 10 | 6.0 | 4.5 |
| 105556 | 1 | 1 | 4 | - | 3 | -1 | 1.9 | 1.4 |
| 105557 | 162 | 189 | 146 | 180 | -16 | -9 | 1.3 | 0.7 |
| 105558 | 5 | 4 | - | - | -5 | -4 | 3.2 | 2.8 |
| 105555 | 18 | 12 | - | - | -18 | -12 | 6.0 | 4.9 |
| 105552 | 10 | 8 | 7 | 3 | -3 | -5 | 1.0 | 2.1 |
| 105553 | 37 | 36 | 4 | 28 | -33 | -8 | 7.3 | 1.4 |
| 105554 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105549 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105544 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105559 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105685 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105682 | - | - | 4 | 2 | 4 | 2 | 2.8 | 2.0 |
| 105683 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106296 | - | - | 1 | - | 1 | 0 | 1.4 | 0.0 |
| 105681 | 18 | 21 | - | - | -18 | -21 | 6.0 | 6.5 |
| 105678 | 310 | 291 | 397 | 387 | 87 | 96 | 4.6 | 5.2 |
| 105675 | 200 | 228 | 165 | 208 | -35 | -20 | 2.6 | 1.4 |
| 106295 | - | - | 3 | 3 | 3 | 3 | 2.4 | 2.4 |
| 105677 | 34 | 18 | - | - | -34 | -18 | 8.2 | 6.0 |
| 105686 | 12 | 11 | - | - | -12 | -11 | 4.9 | 4.7 |
| 105687 | 22 | 7 | 6 | 3 | -16 | -4 | 4.3 | 1.8 |
| 106298 | - | 1 | - | 1 | 0 | 0 | 0.0 | 0.0 |
| 105689 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 106297 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105679 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105674 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105630 | 20 | 16 | 5 | - | -15 | -16 | 4.2 | 5.7 |
| 105631 | 694 | 585 | 729 | 601 | 35 | 16 | 1.3 | 0.7 |
| 105628 | 97 | 90 | 91 | 98 | -6 | 8 | 0.6 | 0.8 |
| 105625 | 51 | 71 | 47 | 35 | -4 | -36 | 0.6 | 4.9 |
| 105626 | 13 | 15 | - | - | -13 | -15 | 5.1 | 5.5 |
| 105627 | 57 | 52 | 60 | 35 | 3 | -17 | 0.4 | 2.6 |
| 105636 | 96 | 73 | 93 | 67 | -3 | -6 | 0.3 | 0.7 |
| 105637 | 539 | 679 | 486 | 654 | -53 | -25 | 2.3 | 1.0 |
| 105638 | - | 5 | 3 | 1 | 3 | -4 | 2.4 | 2.3 |
| 105635 | 4 | 11 | 5 | 10 | 1 | -1 | 0.5 | 0.3 |
| 105632 | 14 | 10 | 1 | - | -13 | -10 | 4.7 | 4.5 |
| 105633 | 32 | 42 | - | 24 | -32 | -18 | 8.0 | 3.1 |
| 105634 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105629 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 105624 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 105639 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105857 | 39 | 59 | 51 | 76 | 12 | 17 | 1.8 | 2.1 |
| 105856 | 112 | 104 | 62 | 68 | -50 | -36 | 5.4 | 3.9 |
| 105858 | 133 | 200 | 82 | 161 | -51 | -39 | 4.9 | 2.9 |
| 105860 | 422 | 391 | 425 | 389 | 3 | -2 | 0.1 | 0.1 |
| 105862 | 740 | 668 | 788 | 708 | 48 | 40 | 1.7 | 1.5 |
| 105861 | 113 | 172 | 138 | 137 | 25 | -35 | 2.2 | 2.8 |
| 105863 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105855 | 2 | 3 | - | - | -2 | -3 | 2.0 | 2.4 |
| 105859 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105974 | 51 | 81 | 63 | 113 | 12 | 32 | 1.6 | 3.2 |
| 105972 | 223 | 218 | 228 | 242 | 5 | 24 | 0.3 | 1.6 |
| 105970 | 173 | 196 | 105 | 174 | -68 | -22 | 5.8 | 1.6 |
| 105971 | 11 | 17 | 15 | 19 | 4 | 2 | 1.1 | 0.5 |
| 105975 | 15 | 18 | 27 | 27 | 12 | 9 | 2.6 | 1.9 |
| 105976 | 80 | 80 | 83 | 119 | 3 | 39 | 0.3 | 3.9 |
| 105973 | 1 | 1 | 4 | 3 | 3 | 2 | 1.9 | 1.4 |
| 105969 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105977 | 7 | 5 | - | - | -7 | -5 | 3.7 | 3.2 |
| 106020 | 22 | 37 | 8 | 24 | -14 | -13 | 3.6 | 2.4 |
| 106021 | 23 | 13 | 9 | 5 | -14 | -8 | 3.5 | 2.7 |
| 106018 | 3 | 5 | 7 | 13 | 4 | 8 | 1.8 | 2.7 |
| 106015 | 3 | 3 | 5 | 1 | 2 | -2 | 1.0 | 1.4 |
| 106016 | 91 | 104 | 61 | 107 | -30 | 3 | 3.4 | 0.3 |
| 106017 | 4 | 1 | 1 | - | -3 | -1 | 1.9 | 1.4 |
| 106026 | 5 | 5 | 2 | 3 | -3 | -2 | 1.6 | 1.0 |
| 106027 | 27 | 36 | 14 | 7 | -13 | -29 | 2.9 | 6.3 |
| 106028 | 5 | 5 | 8 | 7 | 3 | 2 | 1.2 | 0.8 |
| 106025 | 2 | 5 | 8 | 15 | 6 | 10 | 2.7 | 3.2 |
| 106022 | 53 | 72 | 49 | 80 | -4 | 8 | 0.6 | 0.9 |
| 106023 | 12 | 15 | 16 | 16 | 4 | 1 | 1.1 | 0.3 |
| 106024 | 5 | 2 | - | - | -5 | -2 | 3.2 | 2.0 |
| 106019 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 106014 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106029 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105908 | 41 | 62 | 40 | 48 | -1 | -14 | 0.2 | 1.9 |
| 105909 | 580 | 508 | 611 | 554 | 31 | 46 | 1.3 | 2.0 |
| 105906 | 15 | 14 | - | - | -15 | -14 | 5.5 | 5.3 |
| 105903 | 9 | 20 | - | - | -9 | -20 | 4.2 | 6.3 |
| 105904 | 34 | 57 | 34 | 59 | 0 | 2 | 0.0 | 0.3 |
| 105905 | 62 | 80 | 57 | 85 | -5 | 5 | 0.6 | 0.6 |
| 105914 | 14 | 22 | 17 | 29 | 3 | 7 | 0.8 | 1.4 |
| 105915 | 322 | 323 | 326 | 315 | 4 | -8 | 0.2 | 0.4 |
| 105916 | 97 | 102 | 121 | 126 | 24 | 24 | 2.3 | 2.2 |
| 105913 | 221 | 204 | 249 | 167 | 28 | -37 | 1.8 | 2.7 |
| 105910 | 81 | 69 | 81 | 110 | 0 | 41 | 0.0 | 4.3 |
| 105911 | 44 | 35 | 28 | 31 | -16 | -4 | 2.7 | 0.7 |
| 105912 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105907 | 3 | 3 | - | - | -3 | -3 | 2.4 | 2.4 |
| 105902 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105917 | 3 | - | - | - | -3 | 0 | 2.4 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 8657 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8658 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8656 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8652 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8650 | 5 | 5 | 3 | 4 | -2 | -1 | 1.0 | 0.5 |
| 8651 | - | 1 | - | 1 | 0 | 0 | 0.0 | 0.0 |
| 8653 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 8655 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8654 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 8648 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 8646 | 3 | 3 | 6 | 2 | 3 | -1 | 1.4 | 0.6 |
| 8649 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8750 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8752 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8753 | 3 | 6 | 3 | 5 | 0 | -1 | 0.0 | 0.4 |
| 8802 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 6970 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 8780 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8782 | 3 | 6 | 6 | 2 | 3 | -4 | 1.4 | 2.0 |
| 7119 | 1 | - | 1 | 1 | 0 | 1 | 0.0 | 1.4 |
| 7118 | 17 | 10 | 18 | 11 | 1 | 1 | 0.2 | 0.3 |
| 7117 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7112 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 7113 | 3 | 5 | 2 | 3 | -1 | -2 | 0.6 | 1.0 |
| 7110 | 10 | 10 | - | - | -10 | -10 | 4.5 | 4.5 |
| 7114 | 11 | 13 | 4 | 6 | -7 | -7 | 2.6 | 2.3 |
| 7115 | 11 | 8 | 9 | 11 | -2 | 3 | 0.6 | 1.0 |
| 7116 | - | - | 1 | 2 | 1 | 2 | 1.4 | 2.0 |
| 7121 | - | - | - | 2 | 0 | 2 | 0.0 | 2.0 |
| 7120 | 5 | 6 | - | - | -5 | -6 | 3.2 | 3.5 |
| 7122 | - | - | 5 | 3 | 5 | 3 | 3.2 | 2.4 |
| 7162 | 1 | - | 1 | 4 | 0 | 4 | 0.0 | 2.8 |
| 7164 | 16 | 9 | 19 | 12 | 3 | 3 | 0.7 | 0.9 |
| 7165 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 7149 | 2 | - | 1 | - | -1 | 0 | 0.8 | 0.0 |
| 7148 | 10 | 8 | 14 | 14 | 4 | 6 | 1.2 | 1.8 |
| 7145 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105919 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105920 | 13 | 15 | - | - | -13 | -15 | 5.1 | 5.5 |
| 105923 | 13 | 19 | - | - | -13 | -19 | 5.1 | 6.2 |
| 105924 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105922 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105921 | 1 | 2 | 1 | - | 0 | -2 | 0.0 | 2.0 |
| 6235 | 2 | 7 | - | - | -2 | -7 | 2.0 | 3.7 |
| 6234 | 12 | 6 | 17 | 15 | 5 | 9 | 1.3 | 2.8 |
| 6233 | 8 | 7 | 12 | 13 | 4 | 6 | 1.3 | 1.9 |
| 6231 | 3 | 1 | 2 | 1 | -1 | 0 | 0.6 | 0.0 |
| 13115 | 6 | 2 | 3 | 1 | -3 | -1 | 1.4 | 0.8 |
| 6237 | 3 | 5 | 1 | 7 | -2 | 2 | 1.4 | 0.8 |
| 11531 | 13 | 11 | 16 | 15 | 3 | 4 | 0.8 | 1.1 |
| 11529 | 31 | 25 | 24 | 17 | -7 | -8 | 1.3 | 1.7 |
| 11532 | 22 | 27 | 20 | 20 | -2 | -7 | 0.4 | 1.4 |
| 11533 | 1 | 3 | 1 | - | 0 | -3 | 0.0 | 2.4 |
| 11535 | - | 2 | 1 | 6 | 1 | 4 | 1.4 | 2.0 |
| 11534 | 10 | 10 | 12 | 13 | 2 | 3 | 0.6 | 0.9 |
| 9844 | 47 | 41 | 39 | 35 | -8 | -6 | 1.2 | 1.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 13205 | 1 | - | 1 | - | 0 | 0 | 0.0 | 0.0 |
| 13203 | 2 | 1 | 1 | - | -1 | -1 | 0.8 | 1.4 |
| 13204 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 13202 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 9846 | 29 | 35 | 32 | 33 | 3 | -2 | 0.5 | 0.3 |
| 105935 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105937 | 38 | 36 | 40 | 36 | 2 | 0 | 0.3 | 0.0 |
| 105931 | - | - | 3 | 1 | 3 | 1 | 2.4 | 1.4 |
| 105933 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105934 | 33 | 38 | 33 | 33 | 0 | -5 | 0.0 | 0.8 |
| 105927 | 7 | 6 | - | - | -7 | -6 | 3.7 | 3.5 |
| 13265 | 33 | 32 | 40 | 36 | 7 | 4 | 1.2 | 0.7 |
| 13266 | 11 | 9 | - | - | -11 | -9 | 4.7 | 4.2 |
| 13268 | 16 | 15 | - | - | -16 | -15 | 5.7 | 5.5 |
| 13267 | 7 | 3 | - | - | -7 | -3 | 3.7 | 2.4 |
| 13262 | 6 | 9 | - | - | -6 | -9 | 3.5 | 4.2 |
| 13261 | 27 | 26 | 36 | 34 | 9 | 8 | 1.6 | 1.5 |
| 13263 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 13264 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 10017 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 7261 | 1 | 6 | 3 | 3 | 2 | -3 | 1.4 | 1.4 |
| 7262 | 42 | 42 | 40 | 35 | -2 | -7 | 0.3 | 1.1 |
| 7260 | 43 | 41 | 38 | 33 | -5 | -8 | 0.8 | 1.3 |
| 7256 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 5943 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 5944 | 42 | 43 | 44 | 36 | 2 | -7 | 0.3 | 1.1 |
| 13473 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 5950 | 1 | 1 | 1 | 3 | 0 | 2 | 0.0 | 1.4 |
| 5949 | 1 | 3 | - | - | -1 | -3 | 1.4 | 2.4 |
| 5951 | 3 | 4 | - | - | -3 | -4 | 2.4 | 2.8 |
| 5948 | 1 | 2 | 1 | - | 0 | -2 | 0.0 | 2.0 |
| 5947 | 39 | 38 | 37 | 32 | -2 | -6 | 0.3 | 1.0 |
| 5946 | 2 | 1 | - | 1 | -2 | 0 | 2.0 | 0.0 |
| 5941 | 1 | 3 | - | 1 | -1 | -2 | 1.4 | 1.4 |
| 5942 | 5 | 4 | - | - | -5 | -4 | 3.2 | 2.8 |
| 5939 | 4 | 4 | - | - | -4 | -4 | 2.8 | 2.8 |
| 105946 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105947 | 39 | 41 | 39 | 32 | 0 | -9 | 0.0 | 1.5 |
| 105945 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105941 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105939 | - | - | 1 | 1 | 1 | 1 | 1.4 | 1.4 |
| 105940 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105948 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105950 | 42 | 39 | 37 | 32 | -5 | -7 | 0.8 | 1.2 |
| 105949 | 4 | 5 | 1 | 3 | -3 | -2 | 1.9 | 1.0 |
| 105943 | 4 | 3 | 5 | 6 | 1 | 3 | 0.5 | 1.4 |
| 105942 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105944 | 2 | 4 | - | 3 | -2 | -1 | 2.0 | 0.5 |
| 7358 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7359 | 10 | 14 | 19 | 19 | 9 | 5 | 2.4 | 1.2 |
| 7361 | 8 | 10 | 3 | 4 | -5 | -6 | 2.1 | 2.3 |
| 7360 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7355 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 7357 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8485 | 1 | 2 | 5 | 17 | 4 | 15 | 2.3 | 4.9 |
| 8483 | 6 | 6 | 1 | 6 | -5 | 0 | 2.7 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 8484 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 8487 | 2 | 2 | - | 1 | -2 | -1 | 2.0 | 0.8 |
| 8488 | 85 | 47 | 70 | 52 | -15 | 5 | 1.7 | 0.7 |
| 8486 | 2 | 3 | - | 1 | -2 | -2 | 2.0 | 1.4 |
| 8481 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8479 | 5 | 6 | 3 | 4 | -2 | -2 | 1.0 | 0.9 |
| 8482 | 2 | 3 | - | - | -2 | -3 | 2.0 | 2.4 |
| 8489 | 3 | 5 | 18 | 12 | 15 | 7 | 4.6 | 2.4 |
| 8491 | 72 | 65 | 82 | 63 | 10 | -2 | 1.1 | 0.3 |
| 8375 | 62 | 55 | 63 | 50 | 1 | -5 | 0.1 | 0.7 |
| 8374 | 5 | 7 | - | - | -5 | -7 | 3.2 | 3.7 |
| 8369 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 8371 | - | - | 6 | 4 | 6 | 4 | 3.5 | 2.8 |
| 8372 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 8373 | 76 | 57 | 82 | 62 | 6 | 5 | 0.7 | 0.6 |
| 8466 | 3 | 4 | 9 | 6 | 6 | 2 | 2.4 | 0.9 |
| 8465 | 19 | 17 | 23 | 19 | 4 | 2 | 0.9 | 0.5 |
| 8463 | 22 | 22 | 17 | 21 | -5 | -1 | 1.1 | 0.2 |
| 8467 | 18 | 15 | 21 | 17 | 3 | 2 | 0.7 | 0.5 |
| 8469 | 41 | 41 | 43 | 37 | 2 | -4 | 0.3 | 0.6 |
| 5954 | 5 | 11 | 4 | 11 | -1 | 0 | 0.5 | 0.0 |
| 8470 | 21 | 22 | 25 | 24 | 4 | 2 | 0.8 | 0.4 |
| 8472 | 13 | 9 | 11 | 7 | -2 | -2 | 0.6 | 0.7 |
| 8475 | 9 | 10 | 13 | 9 | 4 | -1 | 1.2 | 0.3 |
| 8474 | 55 | 48 | 60 | 49 | 5 | 1 | 0.7 | 0.1 |
| 8473 | 10 | 10 | 10 | 4 | 0 | -6 | 0.0 | 2.3 |
| 8355 | - | 3 | 1 | - | 1 | -3 | 1.4 | 2.4 |
| 8353 | - | - | 3 | 5 | 3 | 5 | 2.4 | 3.2 |
| 8354 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 8357 | - | 1 | 1 | - | 1 | -1 | 1.4 | 1.4 |
| 8358 | 60 | 57 | 64 | 54 | 4 | -3 | 0.5 | 0.4 |
| 8351 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 8349 | - | - | 1 | - | 1 | 0 | 1.4 | 0.0 |
| 8352 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8359 | 2 | - | 1 | 2 | -1 | 2 | 0.8 | 2.0 |
| 8361 | 78 | 80 | 79 | 80 | 1 | 0 | 0.1 | 0.0 |
| 8394 | 60 | 50 | 62 | 51 | 2 | 1 | 0.3 | 0.1 |
| 8390 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8392 | 2 | 3 | - | - | -2 | -3 | 2.0 | 2.4 |
| 8395 | 4 | 1 | 2 | 1 | -2 | 0 | 1.2 | 0.0 |
| 8396 | 78 | 75 | 76 | 80 | -2 | 5 | 0.2 | 0.6 |
| 11250 | 57 | 60 | 59 | 60 | 2 | 0 | 0.3 | 0.0 |
| 11249 | 5 | 10 | 1 | 10 | -4 | 0 | 2.3 | 0.0 |
| 11246 | 7 | 14 | 8 | 11 | 1 | -3 | 0.4 | 0.8 |
| 11248 | 4 | 2 | 4 | - | 0 | -2 | 0.0 | 2.0 |
| 11251 | 2 | 2 | - | 4 | -2 | 2 | 2.0 | 1.2 |
| 11252 | 76 | 73 | 77 | 80 | 1 | 7 | 0.1 | 0.8 |
| 7813 | 3 | 7 | 3 | 3 | 0 | -4 | 0.0 | 1.8 |
| 7811 | 8 | 4 | 8 | 5 | 0 | 1 | 0.0 | 0.5 |
| 7814 | 10 | 8 | 9 | 7 | -1 | -1 | 0.3 | 0.4 |
| 7815 | 57 | 63 | 57 | 67 | 0 | 4 | 0.0 | 0.5 |
| 7817 | 80 | 78 | 80 | 82 | 0 | 4 | 0.0 | 0.4 |
| 7816 | 4 | 10 | 5 | 9 | 1 | -1 | 0.5 | 0.3 |
| 105321 | 1 | - | 3 | 8 | 2 | 8 | 1.4 | 4.0 |
| 105322 | 3 | 1 | 3 | 4 | 0 | 3 | 0.0 | 1.9 |
| 105323 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 105320 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105317 | 4 | 2 | 2 | 1 | -2 | -1 | 1.2 | 0.8 |
| 105318 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105315 | 1 | - | 2 | - | 1 | 0 | 0.8 | 0.0 |
| 105316 | 4 | 3 | 4 | 3 | 0 | 0 | 0.0 | 0.0 |
| 105313 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 105310 | - | 1 | 1 | 1 | 1 | 0 | 1.4 | 0.0 |
| 105311 | 4 | 5 | 1 | 3 | -3 | -2 | 1.9 | 1.0 |
| 105312 | - | - | 3 | 3 | 3 | 3 | 2.4 | 2.4 |
| 105309 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105324 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105319 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105314 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105441 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105438 | 7 | 10 | 14 | 10 | 7 | 0 | 2.2 | 0.0 |
| 105439 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105436 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105437 | 5 | 3 | 1 | 4 | -4 | 1 | 2.3 | 0.5 |
| 105434 | - | 2 | 4 | 6 | 4 | 4 | 2.8 | 2.0 |
| 105431 | - | 1 | 1 | 2 | 1 | 1 | 1.4 | 0.8 |
| 105432 | 4 | 4 | 5 | 4 | 1 | 0 | 0.5 | 0.0 |
| 105433 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105442 | 1 | 1 | 4 | 2 | 3 | 1 | 1.9 | 0.8 |
| 105443 | 5 | 7 | 4 | 2 | -1 | -5 | 0.5 | 2.4 |
| 105444 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105445 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105440 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105435 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105430 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105877 | 12 | 14 | - | - | -12 | -14 | 4.9 | 5.3 |
| 105876 | 19 | 12 | 25 | 23 | 6 | 11 | 1.3 | 2.6 |
| 105878 | 12 | 11 | 21 | 20 | 9 | 9 | 2.2 | 2.3 |
| 105880 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105882 | 4 | 2 | 1 | - | -3 | -2 | 1.9 | 2.0 |
| 105881 | 11 | 20 | - | - | -11 | -20 | 4.7 | 6.3 |
| 105875 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105879 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105883 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105520 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105522 | 2 | 7 | 2 | 15 | 0 | 8 | 0.0 | 2.4 |
| 105524 | 1 | 4 | 3 | 5 | 2 | 1 | 1.4 | 0.5 |
| 105523 | 12 | 11 | 15 | 17 | 3 | 6 | 0.8 | 1.6 |
| 105519 | 21 | 14 | 24 | 25 | 3 | 11 | 0.6 | 2.5 |
| 105518 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105517 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105521 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105525 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105579 | 3 | 4 | 1 | 2 | -2 | -2 | 1.4 | 1.2 |
| 105577 | 10 | 13 | 12 | 11 | 2 | -2 | 0.6 | 0.6 |
| 105575 | 6 | 4 | 3 | 4 | -3 | 0 | 1.4 | 0.0 |
| 105576 | 1 | 5 | 3 | 4 | 2 | -1 | 1.4 | 0.5 |
| 105580 | 3 | 3 | 6 | 2 | 3 | -1 | 1.4 | 0.6 |
| 105581 | 4 | 8 | - | - | -4 | -8 | 2.8 | 4.0 |
| 105582 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105578 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105574 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 105602 | 5 | 5 | 2 | 2 | -3 | -3 | 1.6 | 1.6 |
| 106312 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105598 | 2 | - | 1 | 4 | -1 | 4 | 0.8 | 2.8 |
| 105599 | 2 | 4 | 4 | 6 | 2 | 2 | 1.2 | 0.9 |
| 106313 | 6 | 10 | 14 | 10 | 8 | 0 | 2.5 | 0.0 |
| 105604 | 8 | 7 | 4 | 3 | -4 | -4 | 1.6 | 1.8 |
| 105605 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105601 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106311 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105550 | - | - | - | 2 | 0 | 2 | 0.0 | 2.0 |
| 105551 | 2 | 6 | 2 | 15 | 0 | 9 | 0.0 | 2.8 |
| 105548 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105545 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105546 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105547 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105556 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105557 | 2 | 4 | 2 | 6 | 0 | 2 | 0.0 | 0.9 |
| 105558 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105555 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105552 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105553 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105554 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105549 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105544 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105559 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105685 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105682 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105683 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106296 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105681 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 105678 | 2 | 5 | 2 | 17 | 0 | 12 | 0.0 | 3.6 |
| 105675 | 3 | 4 | 2 | 6 | -1 | 2 | 0.6 | 0.9 |
| 106295 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105677 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105686 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105687 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106298 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105689 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106297 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105679 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105674 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105630 | - | 3 | - | - | 0 | -3 | 0.0 | 2.4 |
| 105631 | 20 | 17 | 13 | 13 | -7 | -4 | 1.7 | 1.0 |
| 105628 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 105625 | 1 | 5 | - | - | -1 | -5 | 1.4 | 3.2 |
| 105626 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 105627 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105636 | - | 3 | - | - | 0 | -3 | 0.0 | 2.4 |
| 105637 | 10 | 8 | 3 | 4 | -7 | -4 | 2.7 | 1.6 |
| 105638 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105635 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105632 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105633 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105634 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105629 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105624 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 | 8:30 | 9:30 |
| 105639 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105857 | 1 | 1 | - | 1 | -1 | 0 | 1.4 | 0.0 |
| 105856 | 3 | 4 | - | - | -3 | -4 | 2.4 | 2.8 |
| 105858 | 5 | 8 | - | - | -5 | -8 | 3.2 | 4.0 |
| 105860 | 2 | 3 | 3 | 3 | 1 | 0 | 0.6 | 0.0 |
| 105862 | 11 | 14 | 18 | 19 | 7 | 5 | 1.8 | 1.2 |
| 105861 | 2 | - | 1 | 1 | -1 | 1 | 0.8 | 1.4 |
| 105863 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105855 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105859 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105974 | 4 | 8 | 1 | 3 | -3 | -5 | 1.9 | 2.1 |
| 105972 | 3 | 3 | - | 9 | -3 | 6 | 2.4 | 2.4 |
| 105970 | 5 | 5 | 2 | 5 | -3 | 0 | 1.6 | 0.0 |
| 105971 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105975 | - | 2 | 1 | - | 1 | -2 | 1.4 | 2.0 |
| 105976 | 3 | 3 | 4 | 3 | 1 | 0 | 0.5 | 0.0 |
| 105973 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 105969 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105977 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106020 | - | 4 | - | - | 0 | -4 | 0.0 | 2.8 |
| 106021 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 106018 | - | - | 1 | - | 1 | 0 | 1.4 | 0.0 |
| 106015 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106016 | 1 | 3 | 1 | 3 | 0 | 0 | 0.0 | 0.0 |
| 106017 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 106026 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 106027 | 1 | 3 | - | - | -1 | -3 | 1.4 | 2.4 |
| 106028 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 106025 | 2 | 4 | - | - | -2 | -4 | 2.0 | 2.8 |
| 106022 | 5 | 5 | 1 | - | -4 | -5 | 2.3 | 3.2 |
| 106023 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 106024 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106019 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106014 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106029 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105908 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 105909 | 10 | 10 | 19 | 19 | 9 | 9 | 2.4 | 2.4 |
| 105906 | 1 | 3 | - | - | -1 | -3 | 1.4 | 2.4 |
| 105903 | 3 | 5 | - | - | -3 | -5 | 2.4 | 3.2 |
| 105904 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105905 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105914 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105915 | 2 | 4 | 3 | 4 | 1 | 0 | 0.6 | 0.0 |
| 105916 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105913 | 2 | 4 | - | 2 | -2 | -2 | 2.0 | 1.2 |
| 105910 | 3 | 3 | - | - | -3 | -3 | 2.4 | 2.4 |
| 105911 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105912 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105907 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105902 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105917 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 106372 | 197 | 163 | 196 | 167 | -1 | 4 | 0.1 | 0.3 |
| 106373 | 272 | 260 | 275 | 258 | 3 | -2 | 0.2 | 0.1 |
| 106374 | 42 | 36 | 41 | 41 | -1 | 5 | 0.2 | 0.8 |
| 106375 | 35 | 31 | 34 | 28 | -1 | -3 | 0.2 | 0.6 |
| 106376 | 220 | 218 | 208 | 220 | -12 | 2 | 0.8 | 0.1 |
| 106377 | 171 | 168 | 166 | 182 | -5 | 14 | 0.4 | 1.1 |
| 106378 | 27 | 23 | - | 1 | -27 | -22 | 7.3 | 6.4 |
| 106379 | 21 | 14 | 4 | 6 | -17 | -8 | 4.8 | 2.5 |
| 106380 | 38 | 38 | 42 | 46 | 4 | 8 | 0.6 | 1.2 |
| 106381 | 66 | 82 | 62 | 65 | -4 | -17 | 0.5 | 2.0 |
| 106382 | 14 | 14 | 12 | 12 | -2 | -2 | 0.6 | 0.6 |
| 106383 | 60 | 45 | 8 | 4 | -52 | -41 | 8.9 | 8.3 |
| 106384 | 83 | 74 | 111 | 89 | 28 | 15 | 2.8 | 1.7 |
| 106386 | 27 | 38 | 59 | 39 | 32 | 1 | 4.9 | 0.2 |
| 106385 | 37 | 40 | 44 | 62 | 7 | 22 | 1.1 | 3.1 |
| 106387 | 121 | 87 | 130 | 113 | 9 | 26 | 0.8 | 2.6 |
| 106388 | 88 | 79 | 61 | 51 | -27 | -28 | 3.1 | 3.5 |
| 106389 | 156 | 144 | 134 | 136 | -22 | -8 | 1.8 | 0.7 |
| 106390 | 123 | 104 | 124 | 108 | 1 | 4 | 0.1 | 0.4 |
| 106391 | 91 | 85 | 88 | 114 | -3 | 29 | 0.3 | 2.9 |
| 106392 | 57 | 60 | 62 | 76 | 5 | 16 | 0.6 | 1.9 |
| 106393 | 314 | 352 | 370 | 430 | 56 | 78 | 3.0 | 3.9 |
| 106394 | 401 | 365 | 402 | 342 | 1 | -23 | 0.0 | 1.2 |
| 106395 | 531 | 614 | 543 | 649 | 12 | 35 | 0.5 | 1.4 |
| 106396 | 725 | 738 | 736 | 729 | 11 | -9 | 0.4 | 0.3 |
| 106397 | 1,095 | 1,092 | 1,173 | 1,169 | 78 | 77 | 2.3 | 2.3 |
| 106398 | 1,084 | 1,039 | 1,142 | 1,098 | 58 | 59 | 1.7 | 1.8 |
| 106399 | 1,496 | 1,622 | 1,501 | 1,658 | 5 | 36 | 0.1 | 0.9 |
| 106400 | 1,607 | 1,553 | 1,598 | 1,561 | -9 | 8 | 0.2 | 0.2 |
| 106401 | 843 | 820 | 867 | 869 | 24 | 49 | 0.8 | 1.7 |
| 106402 | 695 | 691 | 705 | 712 | 10 | 21 | 0.4 | 0.8 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 106372 | 6 | 2 | 8 | 4 | 2 | 2 | 0.8 | 1.2 |
| 106373 | 20 | 16 | 14 | 16 | -6 | 0 | 1.5 | 0.0 |
| 106374 | 2 | 1 | 6 | 5 | 4 | 4 | 2.0 | 2.3 |
| 106375 | 5 | 4 | 2 | - | -3 | -4 | 1.6 | 2.8 |
| 106376 | 1 | 2 | 3 | 2 | 2 | 0 | 1.4 | 0.0 |
| 106377 | 5 | 5 | 9 | 1 | 4 | -4 | 1.5 | 2.3 |
| 106378 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 106379 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 106380 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 106381 | 4 | 3 | - | - | -4 | -3 | 2.8 | 2.4 |
| 106382 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106383 | 10 | 5 | - | - | -10 | -5 | 4.5 | 3.2 |
| 106384 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106386 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 106385 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 106387 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 106388 | 3 | 20 | - | - | -3 | -20 | 2.4 | 6.3 |
| 106389 | 2 | 4 | - | - | -2 | -4 | 2.0 | 2.8 |
| 106390 | 5 | 8 | - | - | -5 | -8 | 3.2 | 4.0 |
| 106391 | 3 | 1 | - | - | -3 | -1 | 2.4 | 1.4 |
| 106392 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 106393 | 14 | 31 | 4 | - | -10 | -31 | 3.3 | 7.9 |
| 106394 | 16 | 14 | 1 | - | -15 | -14 | 5.1 | 5.3 |
| 106395 | 24 | 31 | 21 | 17 | -3 | -14 | 0.6 | 2.9 |
| 106396 | 41 | 38 | 29 | 30 | -12 | -8 | 2.0 | 1.4 |
| 106397 | 51 | 36 | 34 | 23 | -17 | -13 | 2.6 | 2.4 |
| 106398 | 106 | 69 | 73 | 59 | -33 | -10 | 3.5 | 1.3 |
| 106399 | 33 | 21 | 34 | 22 | 1 | 1 | 0.2 | 0.2 |
| 106400 | 40 | 44 | 39 | 45 | -1 | 1 | 0.2 | 0.1 |
| 106401 | 31 | 23 | 29 | 27 | -2 | 4 | 0.4 | 0.8 |
| 106402 | 19 | 22 | 23 | 19 | 4 | -3 | 0.9 | 0.7 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 8657 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8658 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8656 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8652 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8650 | 352 | 382 | 364 | 349 | 12 | -33 | 0.6 | 1.7 |
| 8651 | 33 | 34 | 53 | 43 | 20 | 9 | 3.0 | 1.5 |
| 8653 | 43 | 42 | 7 | - | -36 | -42 | 7.2 | 9.2 |
| 8655 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 8654 | 46 | 36 | 44 | 35 | -2 | -1 | 0.3 | 0.2 |
| 8648 | 30 | 29 | 24 | 13 | -6 | -16 | 1.2 | 3.5 |
| 8646 | 371 | 349 | 401 | 369 | 30 | 20 | 1.5 | 1.1 |
| 8649 | 1 | 1 | 2 | 1 | 1 | 0 | 0.8 | 0.0 |
| 8750 | 23 | 26 | 22 | 27 | -1 | 1 | 0.2 | 0.2 |
| 8752 | 7 | 8 | 5 | 3 | -2 | -5 | 0.8 | 2.1 |
| 8753 | 340 | 363 | 396 | 364 | 56 | 1 | 2.9 | 0.1 |
| 8802 | 91 | 76 | 70 | 64 | -21 | -12 | 2.3 | 1.4 |
| 6970 | 100 | 76 | 98 | 80 | -2 | 4 | 0.2 | 0.5 |
| 8780 | 18 | 13 | - | 3 | -18 | -10 | 6.0 | 3.5 |
| 8782 | 379 | 358 | 410 | 365 | 31 | 7 | 1.6 | 0.4 |
| 7119 | 15 | 12 | 20 | 7 | 5 | -5 | 1.2 | 1.6 |
| 7118 | 288 | 327 | 313 | 327 | 25 | 0 | 1.4 | 0.0 |
| 7117 | 16 | 15 | 5 | 5 | -11 | -10 | 3.4 | 3.2 |
| 7112 | 8 | 15 | 7 | 5 | -1 | -10 | 0.4 | 3.2 |
| 7113 | 144 | 173 | 100 | 121 | -44 | -52 | 4.0 | 4.3 |
| 7110 | 111 | 105 | 95 | 96 | -16 | -9 | 1.6 | 0.9 |
| 7114 | 151 | 173 | 150 | 182 | -1 | 9 | 0.1 | 0.7 |
| 7115 | 338 | 335 | 354 | 361 | 16 | 26 | 0.9 | 1.4 |
| 7116 | 114 | 121 | 100 | 110 | -14 | -11 | 1.4 | 1.0 |
| 7121 | 48 | 61 | 42 | 82 | -6 | 21 | 0.9 | 2.5 |
| 7120 | 174 | 159 | 155 | 144 | -19 | -15 | 1.5 | 1.2 |
| 7122 | 12 | 16 | 33 | 23 | 21 | 7 | 4.4 | 1.6 |
| 7162 | 9 | 9 | 9 | 14 | 0 | 5 | 0.0 | 1.5 |
| 7164 | 287 | 337 | 313 | 319 | 26 | -18 | 1.5 | 1.0 |
| 7165 | 45 | 39 | 19 | 43 | -26 | 4 | 4.6 | 0.6 |
| 7149 | 26 | 27 | 39 | 29 | 13 | 2 | 2.3 | 0.4 |
| 7148 | 330 | 346 | 361 | 359 | 31 | 13 | 1.7 | 0.7 |
| 7145 | 29 | 29 | 29 | 14 | 0 | -15 | 0.0 | 3.2 |
| 105919 | 86 | 73 | 72 | 77 | -14 | 4 | 1.6 | 0.5 |
| 105920 | 244 | 280 | 253 | 277 | 9 | -3 | 0.6 | 0.2 |
| 105923 | 313 | 327 | 330 | 348 | 17 | 21 | 0.9 | 1.1 |
| 105924 | 12 | 14 | - | - | -12 | -14 | 4.9 | 5.3 |
| 105922 | 10 | 12 | - | - | -10 | -12 | 4.5 | 4.9 |
| 105921 | 55 | 50 | 47 | 29 | -8 | -21 | 1.1 | 3.3 |
| 6235 | 266 | 236 | 346 | 342 | 80 | 106 | 4.6 | 6.2 |
| 6234 | 177 | 210 | 176 | 213 | -1 | 3 | 0.1 | 0.2 |
| 6233 | 193 | 201 | 192 | 189 | -1 | -12 | 0.1 | 0.9 |
| 6231 | 174 | 181 | 186 | 212 | 12 | 31 | 0.9 | 2.2 |
| 13115 | 125 | 136 | 144 | 123 | 19 | -13 | 1.6 | 1.1 |
| 6237 | 314 | 303 | 355 | 370 | 41 | 67 | 2.2 | 3.7 |
| 11531 | 306 | 323 | 228 | 334 | -78 | 11 | 4.8 | 0.6 |
| 11529 | 318 | 322 | 228 | 239 | -90 | -83 | 5.4 | 5.0 |
| 11532 | 354 | 381 | 387 | 448 | 33 | 67 | 1.7 | 3.3 |
| 11533 | 143 | 129 | 242 | 193 | 99 | 64 | 7.1 | 5.0 |
| 11535 | 165 | 145 | 185 | 179 | 20 | 34 | 1.5 | 2.7 |
| 11534 | 325 | 360 | 327 | 375 | 2 | 15 | 0.1 | 0.8 |
| 9844 | 515 | 555 | 408 | 523 | -107 | -32 | 5.0 | 1.4 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 13205 | 73 | 108 | 80 | 103 | 7 | -5 | 0.8 | 0.5 |
| 13203 | 47 | 66 | 11 | 9 | -36 | -57 | 6.7 | 9.3 |
| 13204 | 73 | 74 | 5 | 33 | -68 | -41 | 10.9 | 5.6 |
| 13202 | 64 | 75 | 11 | 18 | -53 | -57 | 8.7 | 8.4 |
| 9846 | 569 | 590 | 601 | 640 | 32 | 50 | 1.3 | 2.0 |
| 105935 | 49 | 71 | 39 | 73 | -10 | 2 | 1.5 | 0.2 |
| 105937 | 543 | 625 | 454 | 589 | -89 | -36 | 4.0 | 1.5 |
| 105931 | 55 | 56 | 61 | 59 | 6 | 3 | 0.8 | 0.4 |
| 105933 | 31 | 22 | 17 | 12 | -14 | -10 | 2.9 | 2.4 |
| 105934 | 580 | 633 | 597 | 635 | 17 | 2 | 0.7 | 0.1 |
| 105927 | 37 | 47 | 34 | 40 | -3 | -7 | 0.5 | 1.1 |
| 13265 | 473 | 528 | 430 | 556 | -43 | 28 | 2.0 | 1.2 |
| 13266 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 13268 | 28 | 45 | 15 | 28 | -13 | -17 | 2.8 | 2.8 |
| 13267 | 76 | 105 | 26 | 56 | -50 | -49 | 7.0 | 5.5 |
| 13262 | 166 | 209 | 200 | 234 | 34 | 25 | 2.5 | 1.7 |
| 13261 | 478 | 472 | 460 | 459 | -18 | -13 | 0.8 | 0.6 |
| 13263 | 44 | 51 | 37 | 50 | -7 | -1 | 1.1 | 0.1 |
| 13264 | 35 | 36 | 2 | 2 | -33 | -34 | 7.7 | 7.8 |
| 10017 | 13 | 9 | 3 | 8 | -10 | -1 | 3.5 | 0.3 |
| 7261 | 92 | 103 | 44 | 53 | -48 | -50 | 5.8 | 5.7 |
| 7262 | 410 | 456 | 379 | 491 | -31 | 35 | 1.6 | 1.6 |
| 7260 | 510 | 527 | 489 | 494 | -21 | -33 | 0.9 | 1.5 |
| 7256 | 66 | 74 | 53 | 62 | -13 | -12 | 1.7 | 1.5 |
| 5943 | 62 | 67 | 59 | 51 | -3 | -16 | 0.4 | 2.1 |
| 5944 | 348 | 374 | 314 | 434 | -34 | 60 | 1.9 | 3.0 |
| 13473 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 5950 | 32 | 45 | 28 | 40 | -4 | -5 | 0.7 | 0.8 |
| 5949 | 121 | 136 | 172 | 165 | 51 | 29 | 4.2 | 2.4 |
| 5951 | 90 | 113 | 58 | 70 | -32 | -43 | 3.7 | 4.5 |
| 5948 | 49 | 62 | 24 | 33 | -25 | -29 | 4.1 | 4.2 |
| 5947 | 384 | 398 | 416 | 422 | 32 | 24 | 1.6 | 1.2 |
| 5946 | 79 | 72 | 53 | 41 | -26 | -31 | 3.2 | 4.1 |
| 5941 | 68 | 69 | 47 | 40 | -21 | -29 | 2.8 | 3.9 |
| 5942 | 126 | 128 | 129 | 109 | 3 | -19 | 0.3 | 1.7 |
| 5939 | 154 | 134 | 150 | 103 | -4 | -31 | 0.3 | 2.8 |
| 105946 | 72 | 64 | 73 | 57 | 1 | -7 | 0.1 | 0.9 |
| 105947 | 340 | 329 | 322 | 360 | -18 | 31 | 1.0 | 1.7 |
| 105945 | 32 | 32 | 31 | 28 | -1 | -4 | 0.2 | 0.7 |
| 105941 | 39 | 47 | 34 | 39 | -5 | -8 | 0.8 | 1.2 |
| 105939 | 1 | - | 1 | 9 | 0 | 9 | 0.0 | 4.2 |
| 105940 | - | - | - | 12 | 0 | 12 | 0.0 | 4.9 |
| 105948 | 39 | 47 | 19 | 20 | -20 | -27 | 3.7 | 4.7 |
| 105950 | 466 | 456 | 507 | 474 | 41 | 18 | 1.9 | 0.8 |
| 105949 | 64 | 72 | 68 | 67 | 4 | -5 | 0.5 | 0.6 |
| 105943 | 74 | 91 | 55 | 115 | -19 | 24 | 2.4 | 2.4 |
| 105942 | 33 | 37 | 17 | 23 | -16 | -14 | 3.2 | 2.6 |
| 105944 | 36 | 47 | 33 | 43 | -3 | -4 | 0.5 | 0.6 |
| 7358 | 19 | 22 | 22 | 22 | 3 | 0 | 0.7 | 0.0 |
| 7359 | 583 | 585 | 598 | 580 | 15 | -5 | 0.6 | 0.2 |
| 7361 | 538 | 530 | 533 | 572 | -5 | 42 | 0.2 | 1.8 |
| 7360 | 4 | 8 | 9 | 9 | 5 | 1 | 2.0 | 0.3 |
| 7355 | 35 | 38 | 32 | 35 | -3 | -3 | 0.5 | 0.5 |
| 7357 | 19 | 17 | 15 | 17 | -4 | 0 | 1.0 | 0.0 |
| 8485 | 39 | 33 | 37 | 29 | -2 | -4 | 0.3 | 0.7 |
| 8483 | 315 | 308 | 353 | 351 | 38 | 43 | 2.1 | 2.4 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 8484 | 47 | 58 | 10 | 22 | -37 | -36 | 6.9 | 5.7 |
| 8487 | 62 | 63 | 96 | 61 | 34 | -2 | 3.8 | 0.3 |
| 8488 | 1,016 | 1,023 | 1,053 | 1,023 | 37 | 0 | 1.2 | 0.0 |
| 8486 | 175 | 182 | 156 | 171 | -19 | -11 | 1.5 | 0.8 |
| 8481 | 66 | 71 | 53 | 66 | -13 | -5 | 1.7 | 0.6 |
| 8479 | 390 | 369 | 410 | 398 | 20 | 29 | 1.0 | 1.5 |
| 8482 | 92 | 112 | 90 | 120 | -2 | 8 | 0.2 | 0.7 |
| 8489 | 134 | 128 | 107 | 87 | -27 | -41 | 2.5 | 4.0 |
| 8491 | 1,101 | 1,086 | 1,080 | 1,081 | -21 | -5 | 0.6 | 0.2 |
| 8375 | 1,323 | 1,357 | 1,319 | 1,255 | -4 | -102 | 0.1 | 2.8 |
| 8374 | 3 | 6 | - | - | -3 | -6 | 2.4 | 3.5 |
| 8369 | 80 | 63 | 65 | 56 | -15 | -7 | 1.8 | 0.9 |
| 8371 | 11 | 7 | 19 | 13 | 8 | 6 | 2.1 | 1.9 |
| 8372 | 21 | 18 | 5 | 4 | -16 | -14 | 4.4 | 4.2 |
| 8373 | 1,183 | 1,151 | 1,131 | 1,159 | -52 | 8 | 1.5 | 0.2 |
| 8466 | 109 | 112 | 107 | 110 | -2 | -2 | 0.2 | 0.2 |
| 8465 | 383 | 381 | 407 | 409 | 24 | 28 | 1.2 | 1.4 |
| 8463 | 351 | 327 | 353 | 350 | 2 | 23 | 0.1 | 1.3 |
| 8467 | 126 | 105 | 100 | 79 | -26 | -26 | 2.4 | 2.7 |
| 8469 | 1,062 | 1,053 | 1,064 | 1,007 | 2 | -46 | 0.1 | 1.4 |
| 5954 | 45 | 40 | 79 | 76 | 34 | 36 | 4.3 | 4.7 |
| 8470 | 370 | 353 | 414 | 403 | 44 | 50 | 2.2 | 2.6 |
| 8472 | 98 | 143 | 146 | 137 | 48 | -6 | 4.3 | 0.5 |
| 8475 | 64 | 44 | 19 | 30 | -45 | -14 | 7.0 | 2.3 |
| 8474 | 978 | 946 | 960 | 964 | -18 | 18 | 0.6 | 0.6 |
| 8473 | 199 | 233 | 198 | 220 | -1 | -13 | 0.1 | 0.9 |
| 8355 | 12 | 14 | - | - | -12 | -14 | 4.9 | 5.3 |
| 8353 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8354 | 1 | - | 4 | 5 | 3 | 5 | 1.9 | 3.2 |
| 8357 | 37 | 42 | 34 | 31 | -3 | -11 | 0.5 | 1.8 |
| 8358 | 1,178 | 1,146 | 1,129 | 1,083 | -49 | -63 | 1.4 | 1.9 |
| 8351 | 19 | 23 | 28 | 29 | 9 | 6 | 1.9 | 1.2 |
| 8349 | 1 | - | 8 | 16 | 7 | 16 | 3.3 | 5.7 |
| 8352 | 2 | - | 15 | 11 | 13 | 11 | 4.5 | 4.7 |
| 8359 | 15 | 9 | 16 | 10 | 1 | 1 | 0.3 | 0.3 |
| 8361 | 1,369 | 1,311 | 1,368 | 1,380 | -1 | 69 | 0.0 | 1.9 |
| 8394 | 1,445 | 1,381 | 1,414 | 1,347 | -31 | -34 | 0.8 | 0.9 |
| 8390 | - | - | 10 | 15 | 10 | 15 | 4.5 | 5.5 |
| 8392 | 94 | 101 | 61 | 51 | -33 | -50 | 3.7 | 5.7 |
| 8395 | 30 | 30 | 41 | 40 | 11 | 10 | 1.8 | 1.7 |
| 8396 | 1,339 | 1,330 | 1,348 | 1,387 | 9 | 57 | 0.2 | 1.5 |
| 11250 | 1,403 | 1,306 | 1,391 | 1,298 | -12 | -8 | 0.3 | 0.2 |
| 11249 | 345 | 325 | 350 | 344 | 5 | 19 | 0.3 | 1.0 |
| 11246 | 304 | 272 | 293 | 281 | -11 | 9 | 0.6 | 0.5 |
| 11248 | 102 | 135 | 60 | 64 | -42 | -71 | 4.7 | 7.1 |
| 11251 | 72 | 70 | 57 | 64 | -15 | -6 | 1.9 | 0.7 |
| 11252 | 1,308 | 1,301 | 1,319 | 1,348 | 11 | 47 | 0.3 | 1.3 |
| 7813 | 293 | 255 | 292 | 263 | -1 | 8 | 0.1 | 0.5 |
| 7811 | 185 | 237 | 178 | 241 | -7 | 4 | 0.5 | 0.3 |
| 7814 | 147 | 164 | 146 | 166 | -1 | 2 | 0.1 | 0.2 |
| 7815 | 1,460 | 1,389 | 1,453 | 1,402 | -7 | 13 | 0.2 | 0.3 |
| 7817 | 1,311 | 1,385 | 1,318 | 1,426 | 7 | 41 | 0.2 | 1.1 |
| 7816 | 235 | 213 | 254 | 218 | 19 | 5 | 1.2 | 0.3 |
| 105321 | 9 | 13 | 12 | 18 | 3 | 5 | 0.9 | 1.3 |
| 105322 | 74 | 58 | 71 | 62 | -3 | 4 | 0.4 | 0.5 |
| 105323 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 105320 | 4 | - | - | - | -4 | 0 | 2.8 | 0.0 |
| 105317 | 21 | 17 | 25 | 17 | 4 | 0 | 0.8 | 0.0 |
| 105318 | 32 | 23 | 32 | 26 | 0 | 3 | 0.0 | 0.6 |
| 105315 | 37 | 47 | 34 | 45 | -3 | -2 | 0.5 | 0.3 |
| 105316 | 103 | 98 | 110 | 95 | 7 | -3 | 0.7 | 0.3 |
| 105313 | 69 | 71 | 73 | 68 | 4 | -3 | 0.5 | 0.4 |
| 105310 | 48 | 36 | 45 | 33 | -3 | -3 | 0.4 | 0.5 |
| 105311 | 34 | 22 | 35 | 21 | 1 | -1 | 0.2 | 0.2 |
| 105312 | 4 | 9 | 6 | 16 | 2 | 7 | 0.9 | 2.0 |
| 105309 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105324 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105319 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105314 | 2 | 6 | - | - | -2 | -6 | 2.0 | 3.5 |
| 105441 | 9 | 10 | 6 | 4 | -3 | -6 | 1.1 | 2.3 |
| 105438 | 331 | 301 | 341 | 332 | 10 | 31 | 0.5 | 1.7 |
| 105439 | 25 | 33 | 18 | 27 | -7 | -6 | 1.5 | 1.1 |
| 105436 | 65 | 62 | 16 | 13 | -49 | -49 | 7.7 | 8.0 |
| 105437 | 149 | 162 | 153 | 166 | 4 | 4 | 0.3 | 0.3 |
| 105434 | 43 | 44 | 50 | 53 | 7 | 9 | 1.0 | 1.3 |
| 105431 | 73 | 72 | 95 | 88 | 22 | 16 | 2.4 | 1.8 |
| 105432 | 368 | 378 | 367 | 389 | -1 | 11 | 0.1 | 0.6 |
| 105433 | 29 | 28 | 27 | 33 | -2 | 5 | 0.4 | 0.9 |
| 105442 | 48 | 60 | 47 | 67 | -1 | 7 | 0.1 | 0.9 |
| 105443 | 133 | 147 | 129 | 146 | -4 | -1 | 0.3 | 0.1 |
| 105444 | 19 | 17 | 18 | 11 | -1 | -6 | 0.2 | 1.6 |
| 105445 | 1 | 3 | - | - | -1 | -3 | 1.4 | 2.4 |
| 105440 | - | 3 | - | - | 0 | -3 | 0.0 | 2.4 |
| 105435 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105430 | 3 | 1 | - | - | -3 | -1 | 2.4 | 1.4 |
| 105877 | 149 | 152 | 139 | 105 | -10 | -47 | 0.8 | 4.1 |
| 105876 | 318 | 313 | 279 | 216 | -39 | -97 | 2.3 | 6.0 |
| 105878 | 328 | 326 | 446 | 340 | 118 | 14 | 6.0 | 0.8 |
| 105880 | 189 | 208 | 186 | 153 | -3 | -55 | 0.2 | 4.1 |
| 105882 | 201 | 201 | 191 | 138 | -10 | -63 | 0.7 | 4.8 |
| 105881 | 166 | 185 | 186 | 144 | 20 | -41 | 1.5 | 3.2 |
| 105875 | 14 | 5 | - | - | -14 | -5 | 5.3 | 3.2 |
| 105879 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 105883 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105520 | 52 | 42 | 61 | 56 | 9 | 14 | 1.2 | 2.0 |
| 105522 | 192 | 252 | 239 | 253 | 47 | 1 | 3.2 | 0.1 |
| 105524 | 285 | 291 | 274 | 197 | -11 | -94 | 0.7 | 6.0 |
| 105523 | 431 | 447 | 460 | 349 | 29 | -98 | 1.4 | 4.9 |
| 105519 | 417 | 436 | 361 | 283 | -56 | -153 | 2.8 | 8.1 |
| 105518 | 49 | 24 | 47 | 19 | -2 | -5 | 0.3 | 1.1 |
| 105517 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105521 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105525 | 4 | 9 | - | - | -4 | -9 | 2.8 | 4.2 |
| 105579 | 290 | 309 | 296 | 175 | 6 | -134 | 0.4 | 8.6 |
| 105577 | 504 | 501 | 583 | 413 | 79 | -88 | 3.4 | 4.1 |
| 105575 | 564 | 554 | 599 | 496 | 35 | -58 | 1.5 | 2.5 |
| 105576 | 212 | 205 | 212 | 181 | 0 | -24 | 0.0 | 1.7 |
| 105580 | 226 | 202 | 227 | 172 | 1 | -30 | 0.1 | 2.2 |
| 105581 | 299 | 290 | 300 | 200 | 1 | -90 | 0.1 | 5.7 |
| 105582 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 105578 | 2 | 3 | - | - | -2 | -3 | 2.0 | 2.4 |
| 105574 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 105602 | 386 | 375 | 435 | 361 | 49 | -14 | 2.4 | 0.7 |
| 106312 | 31 | 40 | 81 | 64 | 50 | 24 | 6.7 | 3.3 |
| 105598 | 52 | 60 | 51 | 48 | -1 | -12 | 0.1 | 1.6 |
| 105599 | 398 | 389 | 380 | 311 | -18 | -78 | 0.9 | 4.2 |
| 106313 | 342 | 320 | 348 | 250 | 6 | -70 | 0.3 | 4.1 |
| 105604 | 393 | 382 | 458 | 340 | 65 | -42 | 3.2 | 2.2 |
| 105605 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105601 | 3 | 1 | - | - | -3 | -1 | 2.4 | 1.4 |
| 106311 | 1 | 4 | - | - | -1 | -4 | 1.4 | 2.8 |
| 105550 | 44 | 62 | 42 | 46 | -2 | -16 | 0.3 | 2.2 |
| 105551 | 221 | 269 | 283 | 293 | 62 | 24 | 3.9 | 1.4 |
| 105548 | 32 | 21 | 20 | 4 | -12 | -17 | 2.4 | 4.8 |
| 105545 | 18 | 27 | 7 | 6 | -11 | -21 | 3.1 | 5.2 |
| 105546 | 10 | 10 | - | 2 | -10 | -8 | 4.5 | 3.3 |
| 105547 | 2 | 2 | 17 | 18 | 15 | 16 | 4.9 | 5.1 |
| 105556 | - | 2 | 6 | 5 | 6 | 3 | 3.5 | 1.6 |
| 105557 | 324 | 306 | 316 | 211 | -8 | -95 | 0.4 | 5.9 |
| 105558 | 16 | 19 | - | - | -16 | -19 | 5.7 | 6.2 |
| 105555 | 19 | 27 | - | - | -19 | -27 | 6.2 | 7.3 |
| 105552 | 16 | 17 | 20 | 12 | 4 | -5 | 0.9 | 1.3 |
| 105553 | 79 | 69 | 31 | 24 | -48 | -45 | 6.5 | 6.6 |
| 105554 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 105549 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105544 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105559 | 2 | 4 | - | - | -2 | -4 | 2.0 | 2.8 |
| 105685 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105682 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 105683 | - | 2 | 4 | - | 4 | -2 | 2.8 | 2.0 |
| 106296 | 2 | 1 | 2 | 1 | 0 | 0 | 0.0 | 0.0 |
| 105681 | 32 | 28 | - | - | -32 | -28 | 8.0 | 7.5 |
| 105678 | 293 | 334 | 353 | 322 | 60 | -12 | 3.3 | 0.7 |
| 105675 | 387 | 359 | 391 | 251 | 4 | -108 | 0.2 | 6.2 |
| 106295 | - | 1 | 1 | 3 | 1 | 2 | 1.4 | 1.4 |
| 105677 | 31 | 33 | - | - | -31 | -33 | 7.9 | 8.1 |
| 105686 | 12 | 24 | - | - | -12 | -24 | 4.9 | 6.9 |
| 105687 | 17 | 22 | 16 | 15 | -1 | -7 | 0.2 | 1.6 |
| 106298 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105689 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 106297 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105679 | 4 | 5 | - | - | -4 | -5 | 2.8 | 3.2 |
| 105674 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105630 | 41 | 45 | 44 | 37 | 3 | -8 | 0.5 | 1.2 |
| 105631 | 718 | 712 | 805 | 538 | 87 | -174 | 3.2 | 7.0 |
| 105628 | 90 | 96 | 72 | 62 | -18 | -34 | 2.0 | 3.8 |
| 105625 | 92 | 100 | 55 | 14 | -37 | -86 | 4.3 | 11.4 |
| 105626 | 16 | 23 | 1 | 1 | -15 | -22 | 5.1 | 6.4 |
| 105627 | 83 | 106 | 81 | 64 | -2 | -42 | 0.2 | 4.6 |
| 105636 | 106 | 91 | 111 | 71 | 5 | -20 | 0.5 | 2.2 |
| 105637 | 655 | 744 | 704 | 611 | 49 | -133 | 1.9 | 5.1 |
| 105638 | 6 | 4 | 10 | 2 | 4 | -2 | 1.4 | 1.2 |
| 105635 | 7 | 6 | 9 | 2 | 2 | -4 | 0.7 | 2.0 |
| 105632 | 4 | 6 | - | 1 | -4 | -5 | 2.8 | 2.7 |
| 105633 | 19 | 21 | - | - | -19 | -21 | 6.2 | 6.5 |
| 105634 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105629 | 4 | 1 | - | - | -4 | -1 | 2.8 | 1.4 |
| 105624 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |


| CAR | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 105639 | 3 | 5 | - | - | -3 | -5 | 2.4 | 3.2 |
| 105857 | 111 | 112 | 114 | 85 | 3 | -27 | 0.3 | 2.7 |
| 105856 | 154 | 162 | 103 | 62 | -51 | -100 | 4.5 | 9.4 |
| 105858 | 160 | 150 | 159 | 103 | -1 | -47 | 0.1 | 4.2 |
| 105860 | 594 | 579 | 635 | 500 | 41 | -79 | 1.7 | 3.4 |
| 105862 | 615 | 629 | 676 | 525 | 61 | -104 | 2.4 | 4.3 |
| 105861 | 184 | 176 | 165 | 101 | -19 | -75 | 1.4 | 6.4 |
| 105863 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105855 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 105859 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 105974 | 118 | 117 | 129 | 106 | 11 | -11 | 1.0 | 1.0 |
| 105972 | 225 | 249 | 268 | 218 | 43 | -31 | 2.7 | 2.0 |
| 105970 | 297 | 319 | 265 | 189 | -32 | -130 | 1.9 | 8.2 |
| 105971 | 14 | 23 | 16 | 21 | 2 | -2 | 0.5 | 0.4 |
| 105975 | 27 | 27 | 38 | 31 | 11 | 4 | 1.9 | 0.7 |
| 105976 | 81 | 67 | 88 | 41 | 7 | -26 | 0.8 | 3.5 |
| 105973 | 4 | 4 | 11 | 8 | 7 | 4 | 2.6 | 1.6 |
| 105969 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105977 | 6 | 4 | - | - | -6 | -4 | 3.5 | 2.8 |
| 106020 | 45 | 40 | 27 | 22 | -18 | -18 | 3.0 | 3.2 |
| 106021 | 31 | 20 | 22 | 13 | -9 | -7 | 1.7 | 1.7 |
| 106018 | 4 | 6 | 6 | 6 | 2 | 0 | 0.9 | 0.0 |
| 106015 | 5 | 5 | 2 | - | -3 | -5 | 1.6 | 3.2 |
| 106016 | 135 | 143 | 113 | 96 | -22 | -47 | 2.0 | 4.3 |
| 106017 | 1 | 3 | 1 | 6 | 0 | 3 | 0.0 | 1.4 |
| 106026 | 12 | 5 | 2 | - | -10 | -5 | 3.8 | 3.2 |
| 106027 | 31 | 32 | 26 | 23 | -5 | -9 | 0.9 | 1.7 |
| 106028 | 10 | 15 | 11 | 9 | 1 | -6 | 0.3 | 1.7 |
| 106025 | 5 | 6 | 10 | 5 | 5 | -1 | 1.8 | 0.4 |
| 106022 | 105 | 81 | 97 | 55 | -8 | -26 | 0.8 | 3.2 |
| 106023 | 28 | 21 | 17 | 11 | -11 | -10 | 2.3 | 2.5 |
| 106024 | - | 4 | - | - | 0 | -4 | 0.0 | 2.8 |
| 106019 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 106014 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106029 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105908 | 75 | 79 | 57 | 54 | -18 | -25 | 2.2 | 3.1 |
| 105909 | 515 | 501 | 539 | 386 | 24 | -115 | 1.0 | 5.5 |
| 105906 | 12 | 23 | - | - | -12 | -23 | 4.9 | 6.8 |
| 105903 | 33 | 27 | - | - | -33 | -27 | 8.1 | 7.3 |
| 105904 | 81 | 96 | 86 | 72 | 5 | -24 | 0.5 | 2.6 |
| 105905 | 117 | 111 | 117 | 92 | 0 | -19 | 0.0 | 1.9 |
| 105914 | 39 | 43 | 36 | 32 | -3 | -11 | 0.5 | 1.8 |
| 105915 | 467 | 477 | 491 | 411 | 24 | -66 | 1.1 | 3.1 |
| 105916 | 208 | 181 | 218 | 151 | 10 | -30 | 0.7 | 2.3 |
| 105913 | 174 | 204 | 181 | 137 | 7 | -67 | 0.5 | 5.1 |
| 105910 | 66 | 63 | 82 | 65 | 16 | 2 | 1.9 | 0.3 |
| 105911 | 32 | 49 | 29 | 39 | -3 | -10 | 0.5 | 1.5 |
| 105912 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105907 | 2 | 4 | - | - | -2 | -4 | 2.0 | 2.8 |
| 105902 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105917 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 8657 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8658 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8656 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8652 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8650 | 3 | 1 | 1 | - | -2 | -1 | 1.4 | 1.4 |
| 8651 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 8653 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8655 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8654 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 8648 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 8646 | 3 | 4 | - | - | -3 | -4 | 2.4 | 2.8 |
| 8649 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8750 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8752 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8753 | 5 | 1 | 1 | - | -4 | -1 | 2.3 | 1.4 |
| 8802 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 6970 | - | 1 | 1 | - | 1 | -1 | 1.4 | 1.4 |
| 8780 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8782 | 3 | 4 | - | - | -3 | -4 | 2.4 | 2.8 |
| 7119 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7118 | 9 | 3 | 10 | 4 | 1 | 1 | 0.3 | 0.5 |
| 7117 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7112 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7113 | 1 | 3 | - | - | -1 | -3 | 1.4 | 2.4 |
| 7110 | 16 | 9 | - | - | -16 | -9 | 5.7 | 4.2 |
| 7114 | 13 | 14 | 6 | - | -7 | -14 | 2.3 | 5.3 |
| 7115 | 3 | 1 | 7 | 4 | 4 | 3 | 1.8 | 1.9 |
| 7116 | - | 1 | 9 | 1 | 9 | 0 | 4.2 | 0.0 |
| 7121 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 7120 | 2 | 2 | - | - | -2 | -2 | 2.0 | 2.0 |
| 7122 | - | - | 2 | 2 | 2 | 2 | 2.0 | 2.0 |
| 7162 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 7164 | 6 | 3 | 9 | 4 | 3 | 1 | 1.1 | 0.5 |
| 7165 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 7149 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7148 | 3 | 4 | 9 | 6 | 6 | 2 | 2.4 | 0.9 |
| 7145 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105919 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105920 | 15 | 12 | - | - | -15 | -12 | 5.5 | 4.9 |
| 105923 | 15 | 14 | - | - | -15 | -14 | 5.5 | 5.3 |
| 105924 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105922 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105921 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 6235 | 5 | 2 | 2 | 2 | -3 | 0 | 1.6 | 0.0 |
| 6234 | 5 | 3 | 9 | 4 | 4 | 1 | 1.5 | 0.5 |
| 6233 | 2 | - | 9 | 3 | 7 | 3 | 3.0 | 2.4 |
| 6231 | 1 | 3 | - | 2 | -1 | -1 | 1.4 | 0.6 |
| 13115 | 2 | 2 | - | - | -2 | -2 | 2.0 | 2.0 |
| 6237 | 2 | 2 | - | - | -2 | -2 | 2.0 | 2.0 |
| 11531 | 7 | 4 | 8 | 4 | 1 | 0 | 0.4 | 0.0 |
| 11529 | 23 | 17 | 17 | 18 | -6 | 1 | 1.3 | 0.2 |
| 11532 | 23 | 22 | 23 | 25 | 0 | 3 | 0.0 | 0.6 |
| 11533 | 3 | 1 | 2 | 2 | -1 | 1 | 0.6 | 0.8 |
| 11535 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 11534 | 5 | 1 | 10 | 3 | 5 | 2 | 1.8 | 1.4 |
| 9844 | 30 | 24 | 25 | 23 | -5 | -1 | 1.0 | 0.2 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 13205 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 13203 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 13204 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 13202 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 9846 | 23 | 20 | 32 | 29 | 9 | 9 | 1.7 | 1.8 |
| 105935 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105937 | 23 | 22 | 25 | 23 | 2 | 1 | 0.4 | 0.2 |
| 105931 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105933 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105934 | 23 | 22 | 32 | 29 | 9 | 7 | 1.7 | 1.4 |
| 105927 | 7 | 5 | - | - | -7 | -5 | 3.7 | 3.2 |
| 13265 | 21 | 20 | 24 | 23 | 3 | 3 | 0.6 | 0.6 |
| 13266 | 17 | 13 | - | - | -17 | -13 | 5.8 | 5.1 |
| 13268 | 13 | 14 | - | - | -13 | -14 | 5.1 | 5.3 |
| 13267 | 2 | 1 | - | - | -2 | -1 | 2.0 | 1.4 |
| 13262 | 3 | - | 1 | - | -2 | 0 | 1.4 | 0.0 |
| 13261 | 20 | 22 | 31 | 30 | 11 | 8 | 2.2 | 1.6 |
| 13263 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 13264 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 10017 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7261 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7262 | 36 | 33 | 24 | 23 | -12 | -10 | 2.2 | 1.9 |
| 7260 | 36 | 36 | 33 | 30 | -3 | -6 | 0.5 | 1.0 |
| 7256 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 5943 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 5944 | 35 | 31 | 24 | 23 | -11 | -8 | 2.0 | 1.5 |
| 13473 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 5950 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 5949 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 5951 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 5948 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 5947 | 37 | 34 | 32 | 30 | -5 | -4 | 0.9 | 0.7 |
| 5946 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 5941 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 5942 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 5939 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105946 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105947 | 33 | 27 | 26 | 22 | -7 | -5 | 1.3 | 1.0 |
| 105945 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105941 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105939 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105940 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105948 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105950 | 31 | 31 | 32 | 30 | 1 | -1 | 0.2 | 0.2 |
| 105949 | 5 | 4 | - | - | -5 | -4 | 3.2 | 2.8 |
| 105943 | 3 | 5 | - | - | -3 | -5 | 2.4 | 3.2 |
| 105942 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105944 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 7358 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7359 | 8 | 7 | 8 | 7 | 0 | 0 | 0.0 | 0.0 |
| 7361 | 11 | 12 | 7 | 14 | -4 | 2 | 1.3 | 0.6 |
| 7360 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7355 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 7357 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8485 | - | 1 | 23 | 10 | 23 | 9 | 6.8 | 3.8 |
| 8483 | 6 | 3 | 4 | 5 | -2 | 2 | 0.9 | 1.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 8484 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8487 | 2 | - | - | 1 | -2 | 1 | 2.0 | 1.4 |
| 8488 | 30 | 33 | 44 | 41 | 14 | 8 | 2.3 | 1.3 |
| 8486 | 2 | 2 | - | 2 | -2 | 0 | 2.0 | 0.0 |
| 8481 | 1 | 1 | 2 | - | 1 | -1 | 0.8 | 1.4 |
| 8479 | 7 | 8 | 1 | 7 | -6 | -1 | 3.0 | 0.4 |
| 8482 | 3 | 2 | 4 | 6 | 1 | 4 | 0.5 | 2.0 |
| 8489 | 1 | 2 | 4 | - | 3 | -2 | 1.9 | 2.0 |
| 8491 | 18 | 18 | 30 | 22 | 12 | 4 | 2.4 | 0.9 |
| 8375 | 40 | 39 | 45 | 43 | 5 | 4 | 0.8 | 0.6 |
| 8374 | 8 | 5 | - | - | -8 | -5 | 4.0 | 3.2 |
| 8369 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8371 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 8372 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8373 | 22 | 19 | 32 | 22 | 10 | 3 | 1.9 | 0.7 |
| 8466 | 3 | 3 | - | 1 | -3 | -2 | 2.4 | 1.4 |
| 8465 | 22 | 14 | 20 | 22 | -2 | 8 | 0.4 | 1.9 |
| 8463 | 6 | 6 | 9 | 4 | 3 | -2 | 1.1 | 0.9 |
| 8467 | 3 | 5 | 2 | 5 | -1 | 0 | 0.6 | 0.0 |
| 8469 | 31 | 28 | 33 | 29 | 2 | 1 | 0.4 | 0.2 |
| 5954 | 7 | 6 | 4 | 7 | -3 | 1 | 1.3 | 0.4 |
| 8470 | 14 | 16 | 16 | 11 | 2 | -5 | 0.5 | 1.4 |
| 8472 | 8 | 9 | 14 | 11 | 6 | 2 | 1.8 | 0.6 |
| 8475 | 8 | 5 | 8 | - | 0 | -5 | 0.0 | 3.2 |
| 8474 | 15 | 10 | 18 | 20 | 3 | 10 | 0.7 | 2.6 |
| 8473 | 2 | 1 | 5 | 3 | 3 | 2 | 1.6 | 1.4 |
| 8355 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 8353 | - | - | 1 | - | 1 | 0 | 1.4 | 0.0 |
| 8354 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8357 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8358 | 31 | 32 | 32 | 36 | 1 | 4 | 0.2 | 0.7 |
| 8351 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8349 | - | - | 2 | - | 2 | 0 | 2.0 | 0.0 |
| 8352 | - | - | 3 | - | 3 | 0 | 2.4 | 0.0 |
| 8359 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8361 | 26 | 22 | 31 | 31 | 5 | 9 | 0.9 | 1.7 |
| 8394 | 36 | 36 | 31 | 36 | -5 | 0 | 0.9 | 0.0 |
| 8390 | - | - | 1 | - | 1 | 0 | 1.4 | 0.0 |
| 8392 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8395 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 8396 | 22 | 22 | 30 | 29 | 8 | 7 | 1.6 | 1.4 |
| 11250 | 36 | 33 | 34 | 34 | -2 | 1 | 0.3 | 0.2 |
| 11249 | 6 | 6 | 5 | 5 | -1 | -1 | 0.4 | 0.4 |
| 11246 | 4 | 2 | - | - | -4 | -2 | 2.8 | 2.0 |
| 11248 | 4 | 1 | 1 | - | -3 | -1 | 1.9 | 1.4 |
| 11251 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 11252 | 28 | 21 | 30 | 22 | 2 | 1 | 0.4 | 0.2 |
| 7813 | 5 | 1 | 4 | - | -1 | -1 | 0.5 | 1.4 |
| 7811 | 3 | 2 | 4 | 2 | 1 | 0 | 0.5 | 0.0 |
| 7814 | 3 | 6 | 3 | 6 | 0 | 0 | 0.0 | 0.0 |
| 7815 | 37 | 38 | 35 | 40 | -2 | 2 | 0.3 | 0.3 |
| 7817 | 30 | 19 | 30 | 21 | 0 | 2 | 0.0 | 0.4 |
| 7816 | 1 | 1 | - | 1 | -1 | 0 | 1.4 | 0.0 |
| 105321 | - | - | 5 | 3 | 5 | 3 | 3.2 | 2.4 |
| 105322 | 1 | 1 | 6 | 5 | 5 | 4 | 2.7 | 2.3 |
| 105323 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 105320 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105317 | 2 | 3 | 2 | - | 0 | -3 | 0.0 | 2.4 |
| 105318 | 1 | 1 | 1 | 1 | 0 | 0 | 0.0 | 0.0 |
| 105315 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105316 | 1 | 1 | 1 | - | 0 | -1 | 0.0 | 1.4 |
| 105313 | 3 | - | 3 | 2 | 0 | 2 | 0.0 | 2.0 |
| 105310 | - | - | 1 | 2 | 1 | 2 | 1.4 | 2.0 |
| 105311 | 2 | 1 | 2 | - | 0 | -1 | 0.0 | 1.4 |
| 105312 | - | - | 3 | 3 | 3 | 3 | 2.4 | 2.4 |
| 105309 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105324 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105319 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105314 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105441 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105438 | 1 | 4 | 5 | 3 | 4 | -1 | 2.3 | 0.5 |
| 105439 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105436 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105437 | 4 | 6 | 9 | 1 | 5 | -5 | 2.0 | 2.7 |
| 105434 | - | - | - | 1 | 0 | 1 | 0.0 | 1.4 |
| 105431 | - | 1 | 2 | - | 2 | -1 | 2.0 | 1.4 |
| 105432 | - | 1 | 7 | 8 | 7 | 7 | 3.7 | 3.3 |
| 105433 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105442 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105443 | 2 | 2 | - | 1 | -2 | -1 | 2.0 | 0.8 |
| 105444 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105445 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105440 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105435 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105430 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105877 | 14 | 10 | - | - | -14 | -10 | 5.3 | 4.5 |
| 105876 | 8 | 8 | 17 | 14 | 9 | 6 | 2.5 | 1.8 |
| 105878 | 15 | 10 | 25 | 18 | 10 | 8 | 2.2 | 2.1 |
| 105880 | 3 | 3 | - | - | -3 | -3 | 2.4 | 2.4 |
| 105882 | 2 | 2 | - | - | -2 | -2 | 2.0 | 2.0 |
| 105881 | 13 | 12 | - | - | -13 | -12 | 5.1 | 4.9 |
| 105875 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105879 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105883 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105520 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105522 | 3 | 2 | 4 | - | 1 | -2 | 0.5 | 2.0 |
| 105524 | 7 | 1 | 3 | 3 | -4 | 2 | 1.8 | 1.4 |
| 105523 | 15 | 12 | 27 | 19 | 12 | 7 | 2.6 | 1.8 |
| 105519 | 10 | 10 | 17 | 14 | 7 | 4 | 1.9 | 1.2 |
| 105518 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105517 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105521 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105525 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105579 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105577 | 2 | 5 | 5 | 5 | 3 | 0 | 1.6 | 0.0 |
| 105575 | 2 | 6 | 5 | 10 | 3 | 4 | 1.6 | 1.4 |
| 105576 | 4 | 1 | 1 | - | -3 | -1 | 1.9 | 1.4 |
| 105580 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 105581 | 2 | 4 | 4 | - | 2 | -4 | 1.2 | 2.8 |
| 105582 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105578 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105574 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
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| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 105602 | 6 | 3 | 1 | 2 | -5 | -1 | 2.7 | 0.6 |
| 106312 | - | 1 | 1 | - | 1 | -1 | 1.4 | 1.4 |
| 105598 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105599 | - | 3 | 5 | 8 | 5 | 5 | 3.2 | 2.1 |
| 106313 | 1 | 3 | 5 | 3 | 4 | 0 | 2.3 | 0.0 |
| 105604 | 4 | 5 | - | 2 | -4 | -3 | 2.8 | 1.6 |
| 105605 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105601 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106311 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105550 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105551 | 5 | 2 | 4 | - | -1 | -2 | 0.5 | 2.0 |
| 105548 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105545 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105546 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105547 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105556 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105557 | 3 | 1 | 3 | 3 | 0 | 2 | 0.0 | 1.4 |
| 105558 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105555 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105552 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105553 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105554 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105549 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105544 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105559 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105685 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105682 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105683 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106296 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105681 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105678 | 5 | - | 4 | - | -1 | 0 | 0.5 | 0.0 |
| 105675 | 6 | 1 | 1 | - | -5 | -1 | 2.7 | 1.4 |
| 106295 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105677 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105686 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105687 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106298 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105689 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106297 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105679 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105674 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105630 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105631 | 4 | 4 | 5 | 5 | 1 | 1 | 0.5 | 0.5 |
| 105628 | 2 | - | - | - | -2 | 0 | 2.0 | 0.0 |
| 105625 | 1 | 4 | - | - | -1 | -4 | 1.4 | 2.8 |
| 105626 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105627 | 1 | - | - | - | -1 | 0 | 1.4 | 0.0 |
| 105636 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105637 | 4 | 7 | 9 | 10 | 5 | 3 | 2.0 | 1.0 |
| 105638 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105635 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105632 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105633 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105634 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105629 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105624 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |


| Truck | Observed |  | Modelled |  | Difference |  | GEH |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ID | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 | 17:15 | 18:15 |
| 105639 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105857 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105856 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105858 | 1 | 1 | - | - | -1 | -1 | 1.4 | 1.4 |
| 105860 | 4 | 9 | 8 | 11 | 4 | 2 | 1.6 | 0.6 |
| 105862 | 7 | 4 | 5 | 5 | -2 | 1 | 0.8 | 0.5 |
| 105861 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 105863 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105855 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105859 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105974 | 3 | 3 | - | - | -3 | -3 | 2.4 | 2.4 |
| 105972 | 4 | - | 4 | - | 0 | 0 | 0.0 | 0.0 |
| 105970 | 3 | 2 | 1 | - | -2 | -2 | 1.4 | 2.0 |
| 105971 | 3 | - | - | - | -3 | 0 | 2.4 | 0.0 |
| 105975 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105976 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105973 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105969 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105977 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106020 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106021 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 106018 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 106015 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106016 | 3 | 1 | - | - | -3 | -1 | 2.4 | 1.4 |
| 106017 | 4 | 1 | - | - | -4 | -1 | 2.8 | 1.4 |
| 106026 | - | 2 | - | - | 0 | -2 | 0.0 | 2.0 |
| 106027 | 3 | - | - | - | -3 | 0 | 2.4 | 0.0 |
| 106028 | 3 | 2 | - | - | -3 | -2 | 2.4 | 2.0 |
| 106025 | 3 | - | - | - | -3 | 0 | 2.4 | 0.0 |
| 106022 | 1 | 2 | - | - | -1 | -2 | 1.4 | 2.0 |
| 106023 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106024 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106019 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106014 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 106029 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105908 | 1 | - | 2 | 2 | 1 | 2 | 0.8 | 2.0 |
| 105909 | 4 | 2 | 5 | 5 | 1 | 3 | 0.5 | 1.6 |
| 105906 | 3 | 4 | - | - | -3 | -4 | 2.4 | 2.8 |
| 105903 | 6 | 4 | - | - | -6 | -4 | 3.5 | 2.8 |
| 105904 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105905 | 3 | - | - | - | -3 | 0 | 2.4 | 0.0 |
| 105914 | - | 1 | - | - | 0 | -1 | 0.0 | 1.4 |
| 105915 | 5 | 7 | 7 | 10 | 2 | 3 | 0.8 | 1.0 |
| 105916 | 1 | 3 | 1 | 1 | 0 | -2 | 0.0 | 1.4 |
| 105913 | 2 | 3 | - | - | -2 | -3 | 2.0 | 2.4 |
| 105910 | 2 | 2 | - | - | -2 | -2 | 2.0 | 2.0 |
| 105911 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105912 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105907 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105902 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |
| 105917 | - | - | - | - | 0 | 0 | 0.0 | 0.0 |

## C. VALIDATION RESULTS

now
Stantec













|  | - - Observed Average -15\% | $\rightarrow$ Observed Average | - Observed Averge $15 \%$ --Modelled Average |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  | - |  |
|  |  | . |  |
|  |  |  |  |
|  |  |  |  |
|  | ${ }^{500}$ |  | 2,000 |




 Cumulave taver mes (s) \%




${ }^{1.500}{ }^{\text {Cumulative Distanc }}$
$3,000 \quad 3,500$

- observed Average $-15 \%$
..... Obsereve Average (Min
$\rightarrow$ Obsered Avera
-     - Observed Average 1 15\%

(
-     - observed Averge -15\%
$-\ldots .$. observed Average (Min
$\rightarrow \rightarrow$ Obsened Average - Obsered Average +


500
${ }^{1,000}$ cum
Cmulative Distance (m) ${ }^{1,500}$
2,000

Observed Average - observed Average $+15 \%$




## D. TRAFFIC SURVEY DATA

now





now Stantec

